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1 Repeated Glacial-Lake Outburst Floods in Patagonia: An Increasing Hazard?

2
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16 17 Abstract

18 Five similar glacial-lake outburst floods (GLOFs) occurred in April, October, December 2008, March and
19 September 2009 in the Northern Patagonia Icefield. On each occasion Cachet 2 Lake, dammed by the
20 Colonia Glacier, released circa 200-million m³ water into the Colonia River. Refilling has occurred rapidly,
21 such that further outbreak floods can be expected. Pipeflow calculations of the subglacial tunnel drainage and
22 1D hydraulic models of the river flood give consistent results, with an estimated peak discharge surpassing
23 3,000 m³s⁻¹. These floods were larger in magnitude than any flood on record, according to gauged data since
24 1963. However, geomorphological analysis of the Colonia valley shows physical evidence of former
25 catastrophic outburst floods from a larger glacial lake, with flood discharges possibly as high as 16,000 m³s⁻¹.
26 Due to potential impacts of climate change on glacier dynamics in the area, jökulhlaups may increase future
27 flood risks for infrastructure and population. This is particularly relevant in view of the current development
28 of hydropower projects in Chilean Patagonia.

29
30 **Keywords:** jökulhlaup; outburst flood; Patagonia; glacial-lake; climate change

31 32 1. Introduction

33 Glacial-lake outburst floods, GLOFs (or jökulhlaups in Icelandic) occur due to the sudden release of
34 lake-water impounded by a glacier. During the 2008-2009 hydrologic year, an unexpected sequence of 5
35 jökulhlaups occurred in the Colonia River valley in Patagonia, Chile (Fig. 1): April 6-7, October 7-8, and
36 December 21-22, 2008; March 4-5 and September 16-17, 2009. Each event drained Cachet 2 Lake, circa 200
37 million m³, and flooded large parts of the Colonia and Baker River valleys, near the town of Cochrane. The
38 April event, for example, caused considerable damage to farm settlements and stock mortalities, and put the
39 town of Caleta Tortel at the mouth of the Baker River at risk.

40
41 Although jökulhlaups have occurred recently in the Patagonian icefields in general (Harrison *et al.*, 2006;
42 Tanaka, 1980; Peña and Escobar, 1983; Andrés Rivera, pers.comm. 2008), the last prior event in the Colonia
43 River basin occurred in the 1960s based in gauge data. The repetitive drainage of Cachet 2 Lake in 2008-
44 2009 is therefore remarkable, after over 40 years without jökulhlaups occurring in the Colonia valley. The
45 lake refilled in progressively shorter times after each of these similar events. Therefore, further outburst
46 floods can be expected soon.

47
48 Jökulhlaup research has mainly focused on their extreme flood flows and modelling (e.g. Alho & Aaltonen
49 2008; Osti & Egashira 2009), while a few studies report that they may contribute with the major part of the
50 sediment flux in glacierized catchments (Desloges & Church 1992; Old *et al.* 2005; Russell *et al.* 2006), and
51 most of them relate to sites in braided sandur plains in Iceland or to moraine breaks in the Himalayas. Severe
52 events have been reported in the Andes, resulting in death losses and damage to infrastructure (e.g. Carey,
53 2005; Peña and Escobar, 1983).

54
55 The Colonia is an outlet glacier located at the eastern side of the North Patagonian Icefield in southern Chile,
56 47°16'S, 73°13'W (Fig. 1). In the upper catchment, both the Colonia and Arco glaciers contribute inflows to
57 Colonia Lake, and dam glacial lakes: Cachet 2 (Colonia Glacier) and Arco (Arco Glacier); these are known to
58 have generated outburst floods in the past (Table 1).

59

60 The combination of enhanced ablation rates, accelerated glacier retreat, and augmented subglacial tunnels due
61 to increased discharge from glaciers, is very likely to contribute to a higher frequency of jökulhlaups (Evans
62 & Clague, 1994; Richardson & Reynolds, 2000). Assessing these risks is particularly important in Patagonia
63 in view of the current development of six large-scale hydropower plants in the area (2,300 MW total output,
64 and 2,400 km of transmission lines), one of which would be located immediately downstream of the
65 confluence of the Colonia and Baker rivers.

66

67 A detailed reconstruction of historical Colonia Glacier evolution by means of dendrochronology and
68 lichenometry was described by Harrison & Winchester (2000) and Winchester & Harrison (2000). These
69 studies report that glacier surface levels began to diminish sometime before 1881, when Arco Lake reached
70 its maximum level and then a large flood occurred. Based on aerial photographs and terrain analysis
71 fieldwork done in 1996 by Harrison & Winchester (2000), retreat recommenced around 1980 totalling 350 m
72 (which compares well with the 400 m retreat estimate by Aniya 2007). They signal calving into Colonia Lake
73 as a significant component of glacier ablation, as opposed to surface melting, and that there is a degree of
74 synchrony between glacier retreat in the western and eastern side of the Northern Patagonia Icefield (NPI),
75 possibly related to precipitation input.

76

77 Current glacier retreat trends in Patagonia (Meier & Dyurgerov 2005; Aniya 2007) coincide with a regional
78 increase in air temperature in the late 1970s evidenced in the instrumental and dendrochronological record
79 (Rasmussen *et al.* 2007; Schneider & Gies, 2004; Villalba *et al.*, 2003; Masiokas *et al.*, 2008).
80 Coincidentally, major jökulhlaups in the southern Andes generally re-started in the 1980s, after almost 2
81 decades without events (Table 1).

82

83 The aim of this work is to report succinctly on multiple events from the same site: pre-historic, historic and
84 modern. We will briefly describe the five repeated 2008-2009 flood events, which indicate a possible return
85 to the pre-1970s jökulhlaup mode and focus on a more specific analysis of the 8 October 2008 event. This
86 analysis was based on gauge data and a field inspection completed 10 days after the event, and the use of
87 several methods to estimate the outburst peak flow in this remote region with scarce data. Finally, we present
88 some evidence of pre-historic jökulhlaups, and consider the implications of future events in the region.

89

90 **2. Methods**

91 The Baker River has been monitored since 1963 by the Dirección General de Aguas of Chile (DGA,
92 the Water Authority). Daily discharge and precipitation data are recorded at the nearest gauging station,
93 located approximately 45 km downstream from the glacier snout. Fig. 1 shows the station's location, whilst
94 Fig. 3 presents flow and temperature data for the three 2008 GLOFs.

95

96 The outburst flood peak on October 8 was estimated (1) from Clague-Mathews relation for jökulhlaups (Ng &
97 Björnsson, 2003); (2) from subglacial tunnel drainage using pipeflow calculations following Walder & Costa
98 (1996); (3) at the Lake Colonia outlet using field evidence of flood water marks and hydraulic computations.

99

100 Clague-Mathews (1973) provide an empirical equation (Ng & Björnsson, 2003), which is a curve fit from 10
101 lake outbursts: $Q_{max} = b V^a$, wherein Q_{max} is peak discharge, in $m^3 s^{-1}$, and V is lake volume drained, in hm^3 ,
102 with $b=75$ and $a=0.67$. This relationship was complemented with the similar formulation reported by Walder
103 & Costa (1996), which was fitted to more data, with $b=46$ and $a=0.66$.

104

105 Walder & Costa (1996) provide a method to estimate the discharge through a lateral breach and for a sub-
106 glacial conduit of circular, near-circular or, roughly, rectangular section (the latter was observed in the
107 Colonia Glacier by visits the day after the October event), such that the following heat transfer equation is
108 valid:

109

$$110 \quad h_T D (T_w - T_i) = 0.065 k_w (T_w - T_i) \left(\frac{\rho_w U \tilde{D}}{\eta_w} \right) \quad (1)$$

111

112 wherein h_T is the heat transfer coefficient, D is the depth of flow, T_w and T_i are the water temperature and ice
113 temperature respectively, k_w is the thermal conductivity of water, ρ_w is the density of water, U is mean water
114 velocity and η_w is the (dynamic) viscosity of water. Equation 1 is then combined with the energy equation. For

115 a rectangular conduit the equivalent conduit diameter is $\tilde{D} = 4DB / (2D + B)$, where B is the breadth of the
116 conduit. The water temperature in the Baker River during the outburst flood was recorded as 4°C (Fig. 3) and
117 the ice temperature can be given as 0°C. Assuming these values for temperature, then values of the unknowns
118 h_T , k_w and ρ_w , which vary according to temperature, follow (see Walder & Costa, 1996) and the equations can
119 be solved for values of D and B .

120
121 The Colonia Lake outlet geometry provides the hydraulic control of floodwater hydrographs downstream
122 (Figs. 1 and 3). The outlet channel is approximately straight and a shallow rectangle in section, with a flat
123 gravel bed, but narrows slightly downstream. With a streamflow of c. $50 \text{ m}^3\text{s}^{-1}$, flow was critical during the
124 field survey. Large boulder lag-deposits in the channel and along the banks are consistent with Manning's n
125 roughness coefficients of 0.045 for the river channel and 0.05 for the overbank areas (Barnes, 1967). A
126 previous study reported a similar value for n (0.042) for the streambed, using the Strickler relation
127 $n = D_{90}^{1/6} / 26$ between roughness n and sediment size (D_{90}) sampled in the stream bed and banks (hidroAysén,
128 2008).

129
130 Given the quasi-uniform geometry, criticality, and limited time in this remote location, only two detailed cross
131 sections were surveyed 200 m apart using GPS. The section furthest downstream (cross section A; Fig. 4C) is
132 where the channel narrows. Flow through the upstream section (cross section B) at the lake outlet was
133 assumed subcritical, with critical flow as a boundary condition at downstream cross section A. Flood water
134 marks left by the October 2008 event (sediment and debris) were surveyed at an elevation of 148-149 m
135 (a.s.l.) at upstream cross section B, and two flood water marks were located at 146 and 148 m along
136 downstream cross section A. Channel slope is 0.01 m m^{-1} . There was no field evidence for significant channel
137 erosion or aggradation during the 2008 floods.

138 139 **3. Results and discussion**

140 *Streamflow data analysis and application of empirical relations for outburst maxima*

141 The total volume of the flood waves registered at the Baker-Colonia gauging station, was around
142 230, 190, 125, 200+ and 200 million m^3 for the April, October, December 2008 (Fig. 3), and March and
143 September 2009 events, respectively, which is consistent with the size of the Cachet 2 Lake: 230 million m^3
144 (Casassa et al. 2008). Peak streamflows at the gauge for the 2008 events were approximately $3,600 \text{ m}^3\text{s}^{-1}$,
145 $3,000 \text{ m}^3\text{s}^{-1}$ and $3,050 \text{ m}^3\text{s}^{-1}$, with associated temperature drops (Fig. 3). The March 2009 event exceeded all
146 of these since just before the gauge was damaged it registered $3,800 \text{ m}^3\text{s}^{-1}$ (the last September 16th peak was
147 $3,100 \text{ m}^3\text{s}^{-1}$). The contribution of the Baker River can be estimated from its discharge on the previous day,
148 since upstream stations showed no significant changes the days before and during the event. This analysis
149 results in peak discharges in the Colonia River at the confluence for the 2008 floods of c. $2,500 \text{ m}^3\text{s}^{-1}$, $2,500$
150 m^3s^{-1} , and $2,000 \text{ m}^3\text{s}^{-1}$, respectively. The March 2009 event must have surpassed $2,800 \text{ m}^3\text{s}^{-1}$, and the current
151 last event on September 2009 had a peak contribution of $2,500 \text{ m}^3\text{s}^{-1}$.

152
153 Using the Clague-Mathews formulation for the 2008 events results in peak discharges around 2,600, 2,500
154 and $1,900 \text{ m}^3\text{s}^{-1}$, respectively, Estimations are significantly lower using Walder & Costa formulation, due to
155 the obvious effect of a lower multiplication coefficient. The difference between outcomes is attributed, as
156 reported in the literature, to the fact that these equations are empirical fits to several case studies, while not
157 related to the site-specific effects of the trigger mechanism and conduit geometry (Roberts, 2005). However,
158 the estimations using the former are consistent with the peak flows computed above for the Colonia at the
159 Baker confluence.

160 161 *Field observations*

162 The planview of the Colonia valley is given in Fig. 1. The direction of the 7 km long outbreak
163 through ice tunnels is indicated on Figs. 1 and 2. Oblique images of Cachet 2 Lake and the glacier surface
164 after the jökulhlaup event of 8 October show no evidence of sediment laden water flowing over the glacier
165 surface from the lake. Rather, photographs show a distinct area of major ice-collapse circa 25 m in width -that
166 is roughly transverse to the direction of the glacier flow- and depth 4 m (Fig. 2; Fernando Guzmán, DGA-
167 Chile, pers. comm. 2008) in the surface of the glacier but extending to the 65 m high ice-wall that impounded
168 the lake. This collapse area narrows rapidly and then is terminated where it intersects with a crevasse. Such
169 areas of linear ice-collapse have been reported subsequent to other jökulhlaups discharging through ice
170 tunnels (Walder & Costa, 1996; Kessler & Anderson, 2004). The presence of a pre-existing sub-glacial
171 conduit or complex of conduits for jökulhlaup drainage is not unreasonable (Mäkinen and Palmu, 2008).

172

173 *Flow calculations*

174 Solving equation 1 with values for D and B of respectively 4 m and 25 m, yields a discharge of circa
175 $2,500 \text{ m}^3\text{s}^{-1}$. Equation 1 is most sensitive to values of D and B . Assuming that the dimensions of the collapse
176 in the ice surface reflect a somewhat larger sub-glacial conduit, Equation 1 is less-well balanced (c. 10% error
177 due to mainly uncertainty in depth), yielding discharges in the range of $3,780$ to $4,550 \text{ m}^3\text{s}^{-1}$ with a pipe flow
178 speed of 25 ms^{-1} . Thus, the pipeflow calculation is roughly consistent with estimations based on the Clague-
179 Mathews equation and streamflow observations further downstream, as reported above.

180
181 Calculations at the outlet of Colonia Lake suggest a higher peak discharge. Since the outlet reach is steep (1.0
182 %) it was safe to assume supercritical slope and thus even a single section would have been enough to
183 estimate peak flow using slope data, regardless of roughness values. Critical flow must occur somewhere at
184 the outlet, we surveyed two sections, and estimated peak flow at each one of them using the high water marks
185 (Fig. 4). Considering also bathymetric uncertainties, peak discharges computations yield $3,100$ - $4,500 \text{ m}^3\text{s}^{-1}$,
186 with a reasonable approximation being the average: $3,800 \text{ m}^3\text{s}^{-1}$.

187
188 *Evidence of previous outburst catastrophic flooding*

189 Field inspection at the outlet of Colonia Lake shows geomorphic evidence of ancient large floods
190 carving the lake outlet (Fig. 4). On the right margin of the Colonia River outlet, these palaeoflood indicators
191 consist of high elevation flood-scoured channelways with vertical banks, filled with imbricated boulders and
192 carved on Pleistocene moraine deposits. On the left margin, a large boulder bar contains 4-5 m diameter
193 imbricated boulders (Fig. 4), indicative of ancient catastrophic outburst floods.

194
195 An estimation of the potential discharges carving these morphologies was done using HEC-RAS both (1) with
196 the current topography and (2) assuming that the entrenched Colonia Lake outlet channel was developed by
197 flood incision, and considering a pre-incision topography with channel elevation matching the boulder bar
198 surface. In scenario 1, a flood discharge of $16,000 \text{ m}^3\text{s}^{-1}$ is required to reach the upper spillway channel
199 bottom placed at the right outlet margin. In scenario 2, the discharge required to reach the high elevation
200 flood channel is $7,500 \text{ m}^3\text{s}^{-1}$. According to Walder and Costa (1996) equations, a peak discharge of $7,500$ -
201 $16,000 \text{ m}^3\text{s}^{-1}$ would require a lake volume of 100 - 450 million m^3 assuming a drain through a subaerial breach,
202 usually at the glacier terminus, and of $2,250$ - $7,000$ million m^3 for a drain through a subglacial tunnel. The
203 only obvious source of water for such a flood is lake Arco (Fig. 1).

204
205 Arco Lake was much larger in the past, as concluded by Harrison & Winchester (2000) and Winchester &
206 Harrison (2001) based on dendrochronology and lichenometry, as well as the horizontal trimline also
207 observed by us: approximately 120 m above the 1996 water level, marked by an abrupt change in plant cover
208 that runs horizontally along both sides of the valley. Arco may be speculated as the potential source of water
209 for the catastrophic flood (Tanaka, 1980) possibly producing much larger floods that would sustain our
210 estimate of a palaeo-discharge surpassing $7,500 \text{ m}^3\text{s}^{-1}$ (Harrison and Winchester, 2000). The lack of old tree
211 vegetation we observed on the boulder bar and on the spillway channel may be indicative of a historical flood
212 carving these landforms.

213
214 *Potential implications for dam safety and life-span in a changing Patagonia*

215 These 5 repeated glacial-lake outburst floods in Patagonia entail further practical safety and risk
216 assessment considerations for the three billion dollar plan to build four hydropower stations on the Baker
217 River (Aysén Hydroelectric Project), one located downstream of the jökulhlaup source. The dam safety check
218 flood (10,000-year flood; ICOLD, 1995) was estimated as $6,724 \text{ m}^3\text{s}^{-1}$ in the Environmental Impact Study for
219 the dams (HidroAysén, 2008), based on a probabilistic frequency analysis of the streamflow gauge record
220 from 1963 till 2007.

221
222 Despite being estimated with a time series lacking the recent outburst floods, the check flood for the dam is
223 considerably higher than those resulting from the 2008 jökulhlaups, taking into consideration Baker baseflow
224 during the events. However, the safety check flood should represent the most extreme flood conditions that
225 the dam structure could support without failure, including a low safety margin. Hence, ancient and historical
226 jökulhlaups herein described (which could range between $7,500$ and $16,000 \text{ m}^3\text{s}^{-1}$) require further
227 investigation before deriving an upper discharge limit.

228
229 Finally, from our aerial flights (e.g. Fig 2) and field reconnaissance, it is evident that the braided Colonia
230 River carries a very large sediment load. At its confluence (Fig. 2), the bed material contributed by the

231 Colonia constricts the Baker to a width of only about 50 m from its average upstream value of about 250 to
232 300 m. Large loads delivered by extreme floods could have important consequences for the life expectancy of
233 the planned reservoir: but, no sediment budgets were carried out in the studies for the dams (HidroAysén,
234 2008). However, estimating sediment transport due to jökulhlaups is a challenging necessity (Desloges &
235 Church 1992; Old et al. 2005; Russell et al. 2006).

236

237 **4. Summary and Conclusions**

238 Five very recent glacial-lake outburst floods (jökulhlaups), briefly reported here, occurred on 7
239 April, 8 October, and 21 December 2008, and on 5 March and 16 September 2009, emptying the Cachet 2
240 Lake in Chilean Patagonia, in each occasion releasing circa 200 million m³ of water into the Colonia River.
241 Reconstruction of the October 2008 flood wave through literature formulations, geomorphological
242 observations and hydraulic simulation of the outbreak, reveal similar results (Table 2): peak flow is estimated
243 between 2,500 and 3,500 m³s⁻¹.

244

245 The consistency gives credibility to the hypothesis that the outbreak occurred through a subglacial tunnel.
246 However, it is surmised that to evacuate a peak flow of circa 3,000 m³s⁻¹ through 7 km of glacier ice, from the
247 lake to the snout of the Colonia Glacier, then the enlarged crevasse must intersect a pre-existing sub-glacial
248 drainage conduit (Kessler & Anderson, 2004). Additionally, given the partial rising-limb gauge record, it can
249 be expected that the event on 5 March 2009 exceeded 4,000 m³s⁻¹.

250

251 These repeated GLOFs are particularly relevant for re-assessing risk estimations for planned infrastructure in
252 Patagonia. There is a dam project proposed immediately downstream where the Colonia River meets the
253 Baker River, part of a 6-dam project. The EIS report (HidroAysén, 2008) proposes a safety check flood
254 (10,000 years return period) between 5,500 and 8,000 m³s⁻¹, and does not estimate the sediment contributions
255 from tributaries to the Baker. Given the magnitude of the outburst floods that occurred before the flow
256 gauging started, this check flood may well underestimate the peak discharges from future jökulhlaup events.
257 The large sediment loads contributed by the Colonia River could also result in increased reservoir
258 sedimentation, affecting the life expectancy of the planned dam. In general, more studies are needed regarding
259 the impact of these recent GLOFs in the water, sediment and nutrient budgets of the river (and fjord)
260 ecosystems, as well as risk to existing and planned human infrastructure in Patagonia.

261

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266

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361 **Symbols**

362 $a, b =$ empirical coefficients for Clague-Mathews and Walder & Costa equations

363 $h =$ head loss

364 $\lambda =$ friction factor

365 $K =$ head loss coefficient

366 $D =$ diameter of conduit

367 $R =$ hydraulic radius $= D/4\Phi$

368 $U =$ bulk flow velocity $= Q/\pi D^2/4\phi$

369 $Q =$ discharge

370 $g =$ acceleration due to gravity

371 $k_s =$ equivalent sand grain roughness for ice walls

372 $\nu =$ kinematic viscosity

373 $Re =$ Reynolds number $= UD/\nu$

374 $\Phi =$ pipe shape factor

Table 1: Selected major historical jökulhlaups in the Southern Andes

Glacier/lake	Volume hm ³	Failures	River (approx. latitude)	Discharge m ³ s ⁻¹	References
Nevado del Plomo	53	1934	Mendoza (33° S)	2,700	Fernández et al. 1985
	35; 21; 20	1985 (Feb; Feb; Mar)	Mendoza	284; 277; 184	Fernández et al. 1985, 1991
Moreno – L. Argentino	2,000; 5,000; 3,800	1953; 1956; 1966	Santa Cruz (49° S)	12,000; 20,000; 15,000	Walder & Costa 1996
Juncal	?	1954	Olivares (33°S)	400	Humberto Peña pers.comm. 2008
Cachapoal	1.5 - 2	1981 (8 floods in 19 days)	Cachapoal (34 °S)	150	Humberto Peña pers.comm. 2008
Manflas	5	1981	Seco, Manflas (28° S)	11,000	Peña & Escobar 1987
Dickson - L. Dickson (SPI)	220; 230; 290	Jan 1982; Dec 1982; Mar 1983	Paine (50 °S)	360; 330; 340	Peña & Escobar, 1983a, b
Calafate (NPI)	?	1987 or 1989	Soler (43 °S)	?	Aniya & Naruse 2001
León (NPI)	1.5 - 2	2000	Los Leones (44 °S)	?	Harrison et al. 2006
Colonia (NPI) - L. Cachet/Arco	100-265?	1896/1897, 1914/1917, 1928-1958	Colonia/Baker (47 °S)	2-day flood Dec- Jan (7 m above normal water)	Tanaka 1980; Winchester & Harrison 2000
		1944... 1953, 1955, 1956, 1958, 1963 11 Jan 1964 and 3 Mar 1966 (+ probably 4 Mar 1965 and 7 Jan 1967, yet smaller floods)	Colonia/Baker	?	c. 2,000 (3,100 in Baker River, baseflow c. 1,200 m ³ s ⁻¹)
Colonia - Cachet2	230	2008 (Apr 7)	Colonia/Baker Lago Cachet 2	c. 2,500 (3,600 in Baker River, baseflow c. 1,100 m ³ s ⁻¹)	This paper, by gauge data and Clague-Mathews formulation
	190	2008 (Oct 8)	Colonia/Baker Lago Cachet 2	c. 2,500 (3,000 in Baker River, baseflow circa 500 m ³ s ⁻¹)	This paper, using relations, gauge data, & hydraulic model
	125	2008 (Dec 21)	Colonia/Baker Lago Cachet 2	c. 2,000 (3,050 in Baker River, baseflow c. 1,050 m ³ s ⁻¹)	This paper, by gauge data and Clague-Mathews formulation
	>200	2009 (Mar 5)	Colonia/Baker Lago Cachet 2	>2,800 (>3,800 Baker, damaged gage, baseflow circa 1,000 m ³ s ⁻¹)	This paper, by stream gage data (incomplete record)
	200	2009 (Sep 16)	Colonia/Baker Lago Cachet 2	c. 2,500	This paper, by gauge data

Notes:

1. Many events also reported in Walder & Costa (1996)

2. NPI: Northern Patagonia Icefield. SPI: Southern Patagonia Icefield

380 Table 2: Estimation results for peak flows for the October 2008 Cachet 2 Lake outburst
 381 flood, Patagonia
 382

	Clague- Mathews (empirical)	Pipeflow (physical)	Hydrograph analysis (data)	Hydraulic (physical)
Most sensitive parameter or variable:	V: 200-230 x 10 ⁶ m ³	D: 3-6 m	Rating curve fit	Cross section geometry
Peak discharge (m ³ s ⁻¹):	2,500	2,700	3,000	3,800
Range:	2,400 -2,800	2,500 – 4,500	2,700 – 3,200	3,100 – 4,500

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385 **Figure captions**

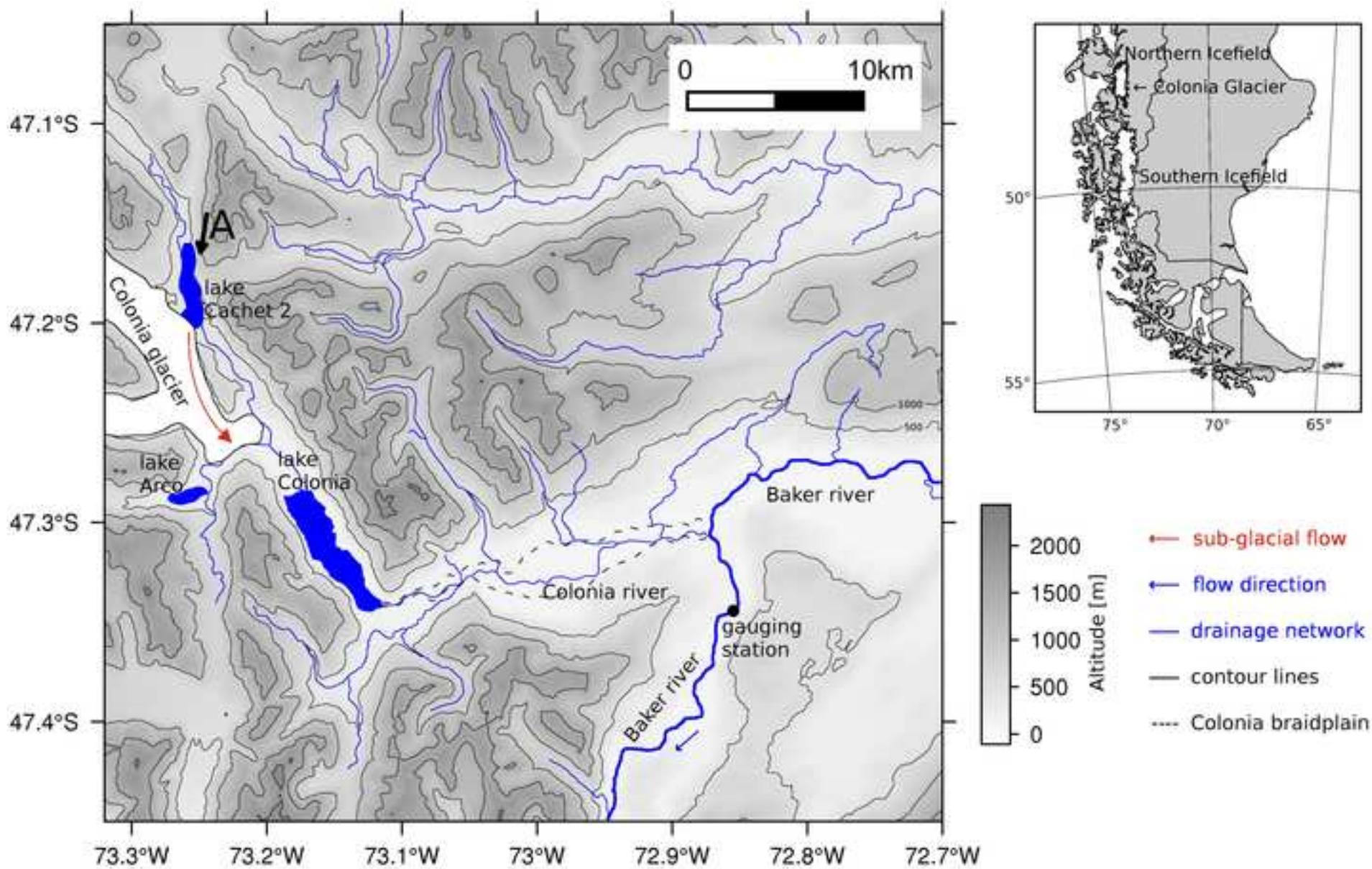
386 Figure 1: Elevation map of the study basin (m). Glaciers are indicated in white. Arrows: flow direction of the
387 jökulhlaups (note arrow detailing viewpoint of aerial photograph 2A). • = location of the DGA hydro-
388 meteorological station on the Baker River

389
390 Figure 2: Aerial photographs of Colonia valley taken 8 October 2008, during the receding period of the
391 jökulhlaup event (17:00-19:00 local time). A: oblique view of Colonia Glacier and empty Cachet 2 Lake,
392 showing drainage point and flow directions (viewpoint detailed in Fig. 1). B: image showing collapsed tunnel.
393 C: Colonia confluence with Baker mainstem during receding flood (source: DGA - Aysén)

394
395 Figure 3: Discharge and water temperature in the Baker-Colonia gage during the jökulhlaup events of April,
396 October and December 2008. Note temperature drops due to Colonia enhanced glacial input to Baker River.

397
398 Figure 4: Lake Colonia outlet reach containing field evidence of 2008 flood water marks and of previous
399 catastrophic flooding. A: Cross-section used on the one-dimensional hydraulic model calculations, showing
400 the flood water level for the 2008 flood(s) and evidences of ancient jökulhlaups (spillway channel and
401 boulder bar). Discharge estimation for the ancient flooding was based both on the current topography, as well
402 as a likely pre-incision topography with channel elevation matching the boulder bar surface (point line
403 between two grey dots). B: Rating curve from hydraulic analysis showing the minimum discharge ranges
404 associated with the 2008 jökulhlaups and with previous palaeoflood stage indicators. C: Upstream view of the
405 Colonia outlet showing the 2008 flood level, the boulder bar and the flood-scoured channelways. D: Boulder
406 bar containing large boulders (4-5 m in diameter) related to high-energy catastrophic outburst floods.
407

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