

1 **Electrochemical synthesis and characterization of basic**
2 **bismuth nitrate $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$: a potential highly**
3 **efficient sorbent for textile reactive dye removal**

4 **Slobodan M. Najdanović¹ · Milica M. Petrović¹ · Miloš M. Kostić¹ ·**
5 **Jelena Z. Mitrović¹ · Danijela V. Bojić¹ · Milan D. Antonijević² ·**
6 **Aleksandar Lj. Bojić¹**

7
8
9 **Abstract**

10 A new method of synthesis was developed for the preparation of basic bismuth
11 nitrate $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$ (ECBBN). Electrochemical synthesis of the
12 material was carried out by galvanostatic electrodeposition from an acidic Bi(III)
13 solution on a Ti substrate and further thermal treatment in air at 200 °C. Charac-
14 terization of ECBBN was conducted by employing SEM–EDX, N_2 adsorption, XRD
15 and FTIR, and its pI was also determined. The analyses showed that the material
16 obtained was pure $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$. Morphologically, ECBBN aggre-
17 gates were composed of crystals, some smaller than 50 nm. Electrochemically syn-
18 thesized sorbent (ECBBN) was used for the removal of the textile dye Reactive Blue
19 19 (RB19) from deionized water and model solutions of polluted river water, and
20 it showed considerably superior sorption performance compared to other inorganic
21 sorbents synthesized by conventional methods reported in the literature. A kinetic
22 study suggests that the sorption process is both under reaction and diffusion con-
23 trol. Equilibration of the sorption process was attained in several minutes, i.e. the
24 sorption process is very fast. The sorption equilibrium data were well interpreted by
25 the Langmuir, Redlich–Peterson and Brouers–Sotolongo isotherm. Using Langmuir
26 isotherm, the maximum sorption capacity of ECBBN was reached at pH 2 and was
27 1049.19 mg g⁻¹.

28 **Keywords** Basic bismuth nitrate · Electrochemical synthesis · Sorption · Textile
29 dye · Reactive Blue 19

A1 ✉ Slobodan M. Najdanović
A2 najda89@gmail.com

A3 ¹ Department of Chemistry, Faculty of Sciences and Mathematics, University of Niš, Višegradska
A4 33, 18000 Niš, Serbia

A5 ² Faculty of Engineering and Science, University of Greenwich at Medway, Central Avenue,
A6 Chatham Maritime, Kent ME4 4TB, England, UK

30 Abbreviations

31	BBN	Basic bismuth nitrate
32	ECBBN	Electrochemically synthesized $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$
33	RB19	Reactive Blue 19
34	pI	Isoelectric point

35 Introduction

36 Synthetic dyes are major industrial pollutants and water contaminants due to their
37 large-scale production and extensive applications [1]. Many industries, such as dye,
38 textile, cosmetic, paper, plastics, leather, rubber, food and pharmaceuticals use dyes
39 to colour their products [2–4]. Significant quantities of synthetic dyes are
40 discharged into the environment from industrial effluents [5]. They give an intense
41 colour to the water and are toxic to the aquatic environment. Hence, wastewater
42 from dye production and industrial applications presents a serious threat to the
43 environment [6, 7]. Reactive Blue 19 (RB19) is an anthraquinone dye, and because
44 it is highly stabilized by resonance, it is very resistant to chemical oxidation [8].
45 Several techniques such as chemical oxidation, biodegradation, photodegradation,
46 electrocoagulation, membrane separation and reverse osmosis have been developed
47 for treating water pollutants [9–13]. There are many studies of photocatalytic
48 degradation of RB19 by different bismuth compounds used as photocatalyst [14–
49 19]. Relative to the foregoing techniques adsorption is considered to be simple,
50 highly efficient and relatively inexpensive, and in a lot of studies, various organic
51 and inorganic compounds are successfully used for removal of RB19 dye [9, 20–
52 27].

53 Basic bismuth nitrates (BBNs) in recent works are used as photocatalysts [28–
54 30] and in rare cases as sorbents [31] for pollutants removal from water. They are
55 also used in medicine for the treatment of gastric and duodenal ulcers, gastritis,
56 dyspepsia, inflamed skin and functional disorders of the large intestine, stomach
57 and duodenum [32]. Typical synthetic methods for the preparation of BBNs
58 include precipitation [31], hydrolysis [30], hydrothermal [28] and microwave-
59 assisted hydrothermal methods [29].

60 Electrodeposition, as one of the most common methods of electrochemical syn-
61 thesis, is very attractive for material synthesis due to its simplicity and ability to
62 easily control of deposition rate, thickness and uniformity of deposit by changing of
63 the electrodeposition process parameters [33]. To our knowledge, electrochemical
64 synthesis of BBNs has not been reported in the scientific literature.

65 The aim of the study reported herein was to develop a new method for the syn-
66 thesis (electrochemical) of basic bismuth nitrate (ECBBN) and to characterize the
67 product by scanning electron microscopy/energy-dispersive X-ray spectroscopy
68 (SEM–EDX), nitrogen sorptometry, X-ray diffraction (XRD) and Fourier trans-
69 form infrared spectroscopy (FTIR) analysis. In addition, the isoelectric point (pI) of
70 the ECBBN was determined. In order to investigate its applicability for textile dye
71 removal, removal of RB19 as a model pollutant in aqueous solutions was evalu-
72 ated, as well as the removal of RB19 from model solutions of polluted river water.
The influence of pH, sorbent dose and initial dye concentration was also examined.

73 Reaction and diffusion kinetics models (pseudo-first-order, pseudo-second-order
74 and intraparticle diffusion), as well as isotherm models (Langmuir, Freundlich,
75 Redlich–Peterson and Brouers–Sotolongo) were examined for a better understand-
76 ing of the sorption process.

77 **Experimental methods**

78 **Materials**

79 Bismuth (III) nitrate pentahydrate was purchased from Acros Organics (USA).
80 Nitric acid, sodium hydroxide, ethanol and RB19 were purchased from Sigma-
81 Aldrich (Germany). All chemicals used in this study were of analytical grade and
82 used without any further purification. Deionized water was used in all experiments.

83 **Synthesis of basic bismuth nitrate**

84 Basic bismuth nitrate was synthesized by electrodeposition from acidic bismuth
85 nitrate solution ($0.1 \text{ mol dm}^{-3} \text{ Bi(NO}_3)_3$ in $1.0 \text{ mol dm}^{-3} \text{ HNO}_3$). Electrodeposition
86 was conducted in a galvanostatic regime at a current density of 150.0 mA cm^{-2} for
87 5.0 min at ambient temperature ($25.0 \pm 0.5 \text{ }^\circ\text{C}$). A conventional two-electrode cell
88 was used for electrodeposition. A sheet of titanium ($10 \times 20 \text{ mm}$) was used as the
89 working electrode (cathode), while stainless-steel sheet ($10 \times 20 \text{ mm}$) was used as
90 the counter electrode (anode). The working and counter electrodes were at a dis-
91 tance of 15 cm. All the electrodes were cleaned before the electrodeposition by pol-
92 ishing with different abrasive papers and ultrasonic cleaning in ethanol and deion-
93 ized water. Electrodeposition was carried out using an Amel 510 DC potentiostat
94 (Materials Mates, Italy) and a VoltaScope software package. After electrodeposi-
95 tion, the titanium sheet with deposited material was dried at room temperature for
96 120 min. Finally, basic bismuth nitrate was obtained by thermal treatment at $200 \text{ }^\circ\text{C}$
97 for 90 min. After cooling in air, the synthesized material was removed from the tita-
98 nium sheet and powdered.

99 **Characterization of sorbent**

100 For SEM–EDX analysis, samples were attached to aluminium stubs using Leit-C car-
101 bon cement. A cold FEG-SEM (SU8030, Hitachi, Japan) was used for imaging the
102 samples with Noran NSS system 7 ultra-dry X-ray detector (Thermo-scientific, USA)
103 for semi-quantitative EDX analysis. Samples were imaged uncoated. Nitrogen adsorp-
104 tion measurements were performed on a Gemini 5 Surface Area Analyser (Micromer-
105 itics, Norcross, Georgia, USA). Before the measurement, the samples were degassed
106 under flowing nitrogen at $40 \text{ }^\circ\text{C}$ for 20 h. The specific surface area was determined
107 using the Brunauer–Emmett–Teller (BET) method [34]. The Barret–Joyner–Halenda
108 (BJH) method was used for pore volume, area and diameter analysis [35]. The crys-
109 tal structure was identified by X-ray diffraction (XRD) using a powder X-ray

110 diffractometer (Ultima IV, Rigaku, Japan). XRD studies of all the powders were con-
 111 ducted using Cu K α radiation ($\lambda = 1.5406$ nm) produced at 40 kV and 40 mA. Experi-
 112 ments were performed in the scan range $2\theta = 5^\circ - 90^\circ$ under 40 kV, 40 mA, using a scan
 113 speed 5° min^{-1} and step size of 0.02° . Before the measurements, angular corrections
 114 were undertaken by using a reference Si standard. FTIR (Fourier transform infrared
 115 spectrometer) spectra were recorded using KBr discs in the range of $400 - 4000 \text{ cm}^{-1}$
 116 using a BOMEM MB-100 (Hartmann & Braun, Canada) FTIR spectrometer. The num-
 117 ber of scans was 16. The isoelectric point of the sorbent was determined by the salt
 118 addition method [36]. NaNO_3 solution (0.1 mol dm^{-3}) was used as an inert electrolyte
 119 and a series of test solutions were prepared by adjusting the pH of 50.0 cm^3 of electro-
 120 lyte in the range $2.0 - 11.0$ using 0.01 mol dm^{-3} HNO_3 and 0.01 mol dm^{-3} NaOH . Then
 121 0.2 g of sorbent was added to each solution, sealed and stirred for 24 h, and the final pH
 122 (pH_f) was measured. The pH_f values were plotted against the initial pH (pH_i), and the
 123 pI was determined from the data where $\text{pH}_i = \text{pH}_f$.

124 Batch sorption experiments

125 Batch sorption experiments were performed to study the effect of parameters such as
 126 contact time, pH, sorbent dose and initial dye concentration, as well as to determine
 127 maximum sorption capacity. The experiments were carried out at ambient temperature
 128 in a Petri dish by adding the desired amount of sorbent in prepared solutions of RB19
 129 and stirred using a magnetic stirrer, and a series of sorption experiments were done
 130 at different operating conditions by changing initial dye concentrations, initial sorb-
 131 ent doses, reaction times and pH of the solution. The pH of the experimental solutions
 132 was adjusted by adding HNO_3 or NaOH . Residual RB19 concentration was determined
 133 through the measurement of the dye solution absorbance at 592 nm by UV-visible
 134 spectrophotometer (UV-1800, Shimadzu, Japan). Before the measuring of absorbance,
 135 sorbent was separated from the solution by filtration using regenerated cellulose mem-
 136 brane filters with a $0.45 \mu\text{m}$ pore size (Agilent Technologies, Germany). The following
 137 equations were utilized for determining the sorbed amount of dye q_t (mg g^{-1}) and the
 138 dye removal efficiency (RE):

$$139 \quad q_t = \frac{c_0 - c_t}{m} \cdot V \quad (1)$$

$$140 \quad RE = \frac{c_0 - c_t}{c_0} \cdot 100\% \quad (2)$$

141 where c_0 and c_t (mg dm^{-3}) are the initial and final concentrations of the RB19, m (g)
 142 is the mass of the sorbent and V (dm^3) is the solution volume.

143 Relative mean deviation (RMD) was calculated by the following equation:

$$144 \quad RMD = \frac{\sum_{i=1}^n |q_{i, \text{exp}} - q_{i, \text{cal}}|}{q_{\text{exp}} \cdot n} \cdot 100\% \quad (3)$$

145 where $q_{i, \text{exp}}$ (mg g^{-1}) is experimentally obtained amount of sorbed dye at the experi-
146 mental point i , $q_{i, \text{cal}}$ (mg g^{-1}) is calculated amount of sorbed dye at the experimental
147 point i by some kinetic or isotherm model and n is a number of the experimental
148 points.

149 In order to find out whether there is any adsorption on the Petri dish walls, control
150 experiments were carried out in the absence of sorbent, and it was concluded
151 that sorption is negligible. The sorption experiments were conducted in triplicate.
152 All calculations of the experimental data and statistical analysis were performed
153 using OriginPro 2016 software (OriginLab Corporation, USA).

154 Results and discussion

155 Characterization of sorbent

156 SEM analysis

157 Figure 1 shows SEM images of the electrochemically synthesized material at dif-
158 ferent magnifications. Figure 1a shows that ECBBN sorbent consists of aggregates
159 below $40 \mu\text{m}$, and it exhibits various shapes and sizes. Some of the aggregates are
160 basically polyhedrons with relatively plane facets, and it is hard to distinguish the
161 particular aggregates. However, there is also a significant part of the surface, which

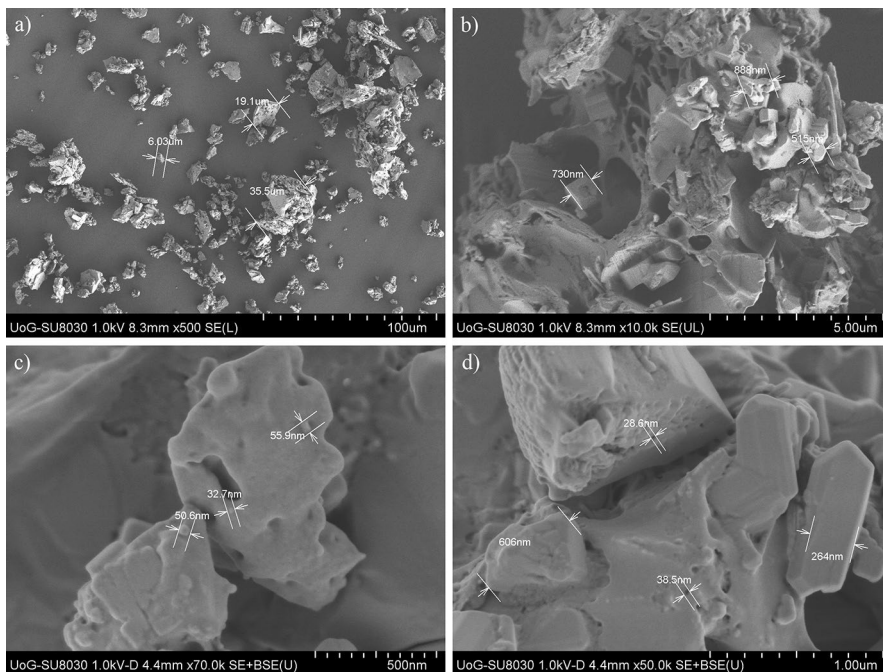


Fig. 1 SEM images of ECBBN at a magnifications of a $\times 500$, b $\times 10,000$, c $\times 70,000$ and d $\times 50,000$

162 appears to be monolithic. Aggregates have porous morphology (Fig. 1b), composed
163 of crystals which are smooth in texture and have a variety of forms. Many of them
164 seem to be sintered, forming much bigger structures. A certain part of the crystals
165 has an irregular structure with plane surface structures which thickness varies
166 between 200 and 800 nm. In Fig. 1c, nanometric crystals with diameter 30–50 nm
167 can be observed. Also, pores smaller than 40 nm in diameter can be detected
168 (Fig. 1d).

169 Textural properties

170 The textural properties of ECBBN sorbent have been studied by the nitrogen adsorp-
171 tion measurements. The nitrogen adsorption/desorption isotherms of ECBBN are
172 shown in Fig. 2. According to IUPAC classification, they belong to the isotherm
173 type II, with a type H3 hysteresis loop in the relative pressure range of 0.9–1.0.
174 Such shape of isotherm indicates unrestricted monolayer adsorption on nonporous
175 or macroporous adsorbents. Hysteresis loop of H3 type is characteristic of non-
176 rigid aggregates of plate-like particles and materials, whose pore network consists
177 of macropores [37]. The BET specific surface area of ECBBN is $0.95 \text{ m}^2 \text{ g}^{-1}$. The
178 BJH analysis shows narrow pores with an average pore diameter of 9.99 nm. The
179 mesopore surface area of ECBBN amounts to $0.69 \text{ m}^2 \text{ g}^{-1}$, while the volume of
180 pores is $0.0017 \text{ cm}^3 \text{ g}^{-1}$.

181 XRD analysis

182 The XRD spectrum of the synthesized ECBBN is presented in Fig. 3. It shows dif-
183 fraction peaks at 11.64° , 12.96° , 20.22° , 23.47° , 27.06° , 34.07° , 41.24° and 52.54°
184 2θ values, which can be indexed to $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$ according to the

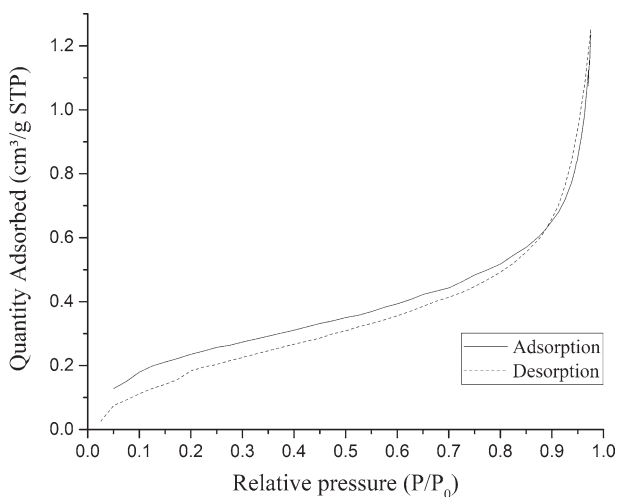


Fig. 2 The N₂ adsorption/desorption isotherm of ECBBN

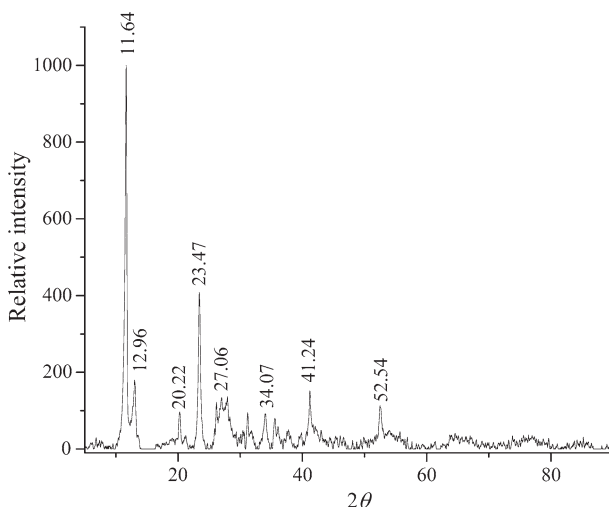


Fig. 3 XRD pattern of ECBBN

185 XRD database JCPDS-ICDD: PDF-2 00-054-0627. The obtained material is composed of trigonal $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$ (space group P-3, $a=b=15.187 \text{ \AA}$,
 186 $c=15.838 \text{ \AA}$, $\alpha=\beta=90^\circ$, $\gamma=120^\circ$). Sharp peaks indicate that the synthesized
 187 $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$ displays high crystallinity. No other phases were found.
 188 By using the Williamson–Hall method [38], it is estimated that the crystallite size of
 189 the material is $11.3 \pm 0.2 \text{ nm}$.
 190

191 EDX analysis

192 EDX analysis (Fig. 4) of electrochemically synthesized material shows the presence
 193 of Bi, O and N, which corresponds to typical BBN composition. The weight per-
 194 centage of elements for ECBBN determined by EDX analysis are given in Table 1,
 195 and the results are in good agreement with the theoretical weight percentages for
 196 $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$.

197 FTIR analysis

198 The FTIR spectral analysis is important to identify the characteristic functional
 199 groups of material. Figure 5 shows the FTIR spectra of ECBBN sorbent. The broad
 200 absorption peak centred at 3421 cm^{-1} is assigned to the stretching vibrations of
 201 $-\text{OH}$ groups [39]. The $-\text{OH}$ bending vibration mode of lattice water corresponds to
 202 the band at 1626 cm^{-1} [40, 41]. The bands appearing at 718, 811, 1036, 1327, 1354
 203 and 1384 cm^{-1} originate from the NO_3^- vibrations and fit well to the data from the
 204 literature [42–44]. The absence of IR bands at 736, 803 and 1297 cm^{-1} is character-
 205 istic for hydrated nitrates [43]. Thus, synthesized ECBBN contains water molecules
 206 in its structure. The bands observed at 563 and 442 cm^{-1} are assigned to the Bi–O

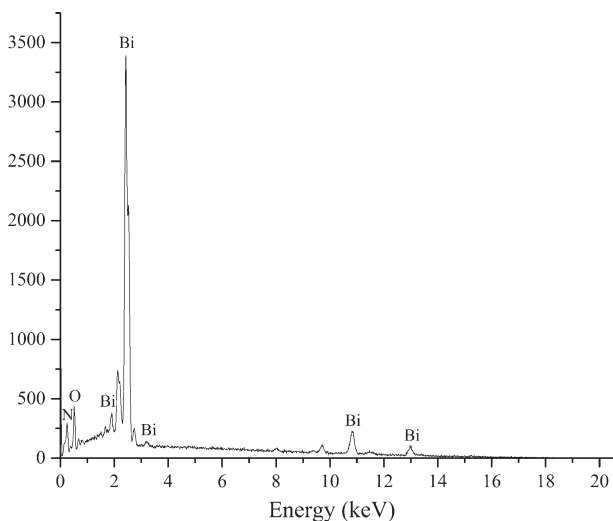


Fig. 4 EDX spectrum of ECBBN

Table 1 Weight percentages of elements in ECBBN by EDX analysis

Element	Experimental weight percentage (%) of elements in ECBBN	Theoretical weight percentage (%) of elements in $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$
Bi	73.26	72.43
O	20.73	23.11
N	6.01	4.04
H	–	0.41

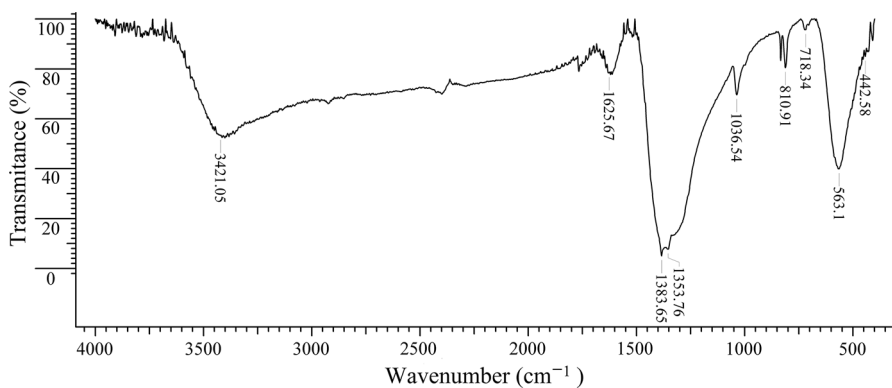


Fig. 5 FTIR spectrum of ECBBN

207 bond stretching vibrations [45, 46]. The FTIR spectrum obtained for the ECBBN
208 corresponds to the spectrum of $[\text{Bi}_6\text{O}_5(\text{OH})_3](\text{NO}_3)_5 \cdot 2\text{H}_2\text{O}$ reported by Christensen
209 et al. [47].

210 The isoelectric point

211 The isoelectric point (pI) of the synthesized ECBBN sorbent determined by the salt
212 addition method is 2.12, which shows that the sorbent is strongly acidic. The sorbent
213 surface is positively charged at $\text{pH} < 2.12$ and negatively charged at $\text{pH} > 2.12$.

214 The ability of ECBBN to remove RB19

215 The ability of the sorbent ECBBN to remove RB19 was studied as a function of
216 time, using an initial sorbent dose of 500.0 mg dm^{-3} , initial RB19 concentration
217 of 500.0 mg dm^{-3} and at native pH. The results (Fig. 6) show that the sorption
218 process occurs in two phases. In the first, initial phase, rapid uptake of RB19 mol-
219 ecules occurs, and during this phase (1 min), more than 95% of the total amount
220 of sorbed dye was removed. The second phase is much slower, and the amount of
221 sorbed dye was less than 5% of the total sorbed amount. From these results, it can
222 be concluded that equilibrium was reached in several minutes, and the maximum
223 amount of sorbed dye at native pH was 838.56 mg g^{-1} . Electrochemically synthe-
224 sized sorbent (ECBBN) exhibits much higher sorption capacity for RB19 than other
225 sorbents, especially than inorganic sorbents synthesized by conventional methods,
226 such as precipitation, coprecipitation and hydrothermal methods, reported in previ-
227 ous studies (Table 2) [20–27]. Another advantage of the electrochemically synthe-
228 sized sorbent is much lower sorption equilibrium time, which makes the sorption

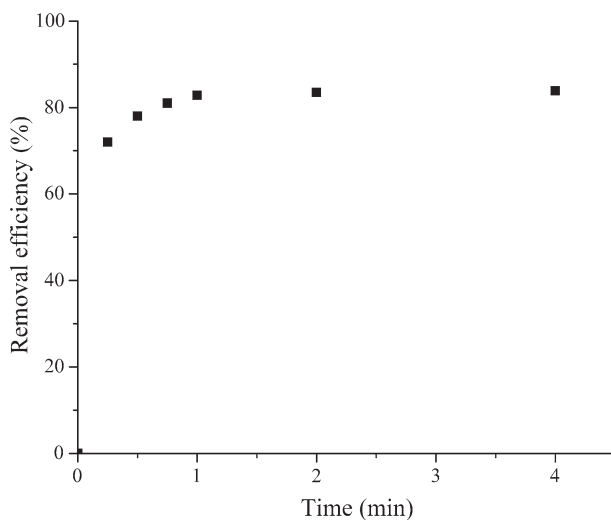
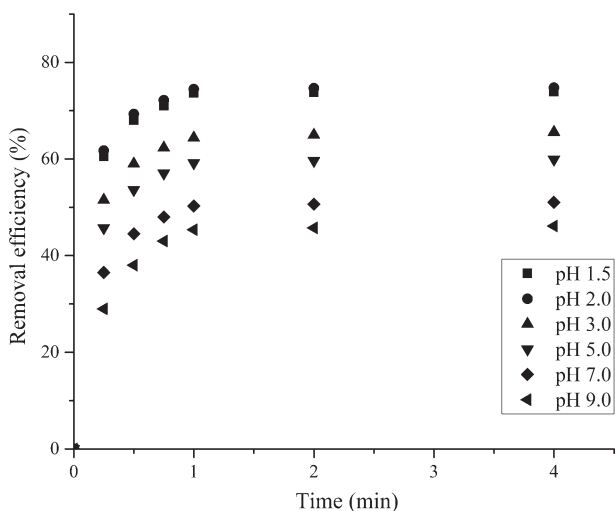


Fig. 6 Effect of contact time on the removal efficiency of RB19. $c_{\text{RB19}} 500.0 \text{ mg dm}^{-3}$, $c_{\text{sorbent}} 500.0 \text{ mg dm}^{-3}$, temperature $25.0 \pm 0.5 \text{ }^\circ\text{C}$, pH native

Table 2 Comparison of sorption capacity of different sorbents for the removal of RB19

Sorbent	Synthesis method	pH	Sorption capacity (mg g ⁻¹)	Equilibrium time (min)	Reference
Magnetite/graphene oxide	Coprecipitation	3.0	62.50	67	[21]
Nanohydroxyapatite	Precipitation	3.0	90.09	180	[20]
NiO nanoparticles	Precipitation	6.5	98.83	15	[22]
Polypyrrole-coated Fe ₃ O ₄	Coprecipitation	3.0	112.36	10	[26]
MgO nanostructures	Hydrothermal	7.8	250.00	20	[23]
Chitosan hollow fibres	–	3.5	454.50	90	[25]
FeCuNi-280	Coprecipitation	2.0	480.80	120	[27]
Chitosan	–	6.8	822.40	150	[24]
ECBBN	Electrochemical	Native pH	838.56	2	This study
ECBBN	Electrochemical	2.0	1046.24	2	This study

**Fig. 7** Effect of pH on the removal efficiency of RB19; c_{RB19} 700.0 mg dm⁻³, c_{sorbent} 500.0 mg dm⁻³, temperature 25.0 ± 0.5 °C

229 process considerably faster. Also, ECBBN has substantially higher sorption ability
230 in comparison with BBN reported by Abdullah et al. [31] which is synthesized with
231 precipitation method and has a sorption capacity of 31 and 24 mg g⁻¹ for Methyl
232 Orange and Sunset Yellow, respectively.

233 Effect of pH on the removal efficiency of RB19

234 The solution pH is another important parameter in sorption controlling because it
235 affects the surface charge of the sorbent and the degree of ionization of the adsorbate

236 [48]. The effect of pH on the removal efficiency of RB19 was evaluated by changing
237 the pH from 1.5 to 9.0. All the experiments were carried out with extremely high con-
238 centration of RB19 (700 mg dm^{-3}) in order to make it easier to see the difference in
239 the removal efficiency of RB19 at different pH values. From the data in Fig. 7, it can
240 be seen that the maximum removal efficiency of RB19 is achieved at pH 1.5 and 2.0,
241 and it decreases with increasing pH. The removal efficiency decreases from 77.73 to
242 46.11%, from pH 2.0 to pH 9.0. At pH 1.5, removal efficiency of ECBBN sorbent is
243 slightly lower than at pH 2.0; therefore, experiments were not conducted at pH values
244 lower than 1.5. Under high acidic conditions (pH 1.5–2.0), the surface of the sorb-
245 ent is positively charged, because the pI of the sorbent is 2.12, and thus the electro-
246 static attraction between the anionic dye RB19 and the sorbent surface is the strong-
247 est at that pH [22]. Therefore, ECBBN has the highest sorption capacity for RB19 at
248 $\text{pH} \leq 2.0$, and it decreases with increasing pH (Fig. 8). The maximum sorption capac-
249 ity at pH 2.0 is $1046.24 \text{ mg g}^{-1}$. Furthermore, the data in Fig. 8 show that in the
250 whole pH range investigated, i.e. at pH 1.5, 2.0, 3.0, 5.0, 7.0 and 9.0, the sorption
251 capacity is high, being 1034.63, 1046.24, 917.47, 838.56, 714.22 and 645.59 mg g^{-1} ,
252 respectively. The minimum sorption capacity is 645.59 mg g^{-1} at pH 9.0, which is
253 still much higher when compared with inorganic sorbents reported in the literature
254 (Table 2). Thus, the high sorption capacity for ECBBN, over the whole investigated
255 pH range, can be considered a beneficial characteristic for the application of the sorb-
256 ent in water treatment, enabling it to be used without the necessity for pH adjustment
257 and the addition of any other chemical component to the sorption system.

258 Effect of sorbent dose on the removal efficiency of RB19

259 The effect of variation in the sorbent dose from 250.0 to $1000.0 \text{ mg dm}^{-3}$ on the
260 removal of RB19 at a constant concentration of RB19 (700.0 mg dm^{-3}) and pH 2

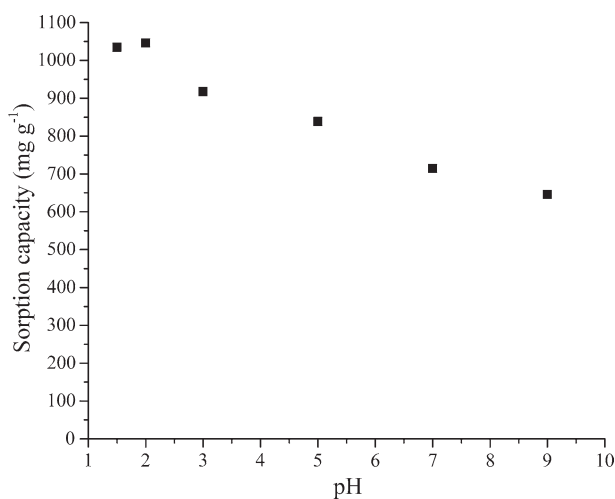


Fig. 8 Sorption capacity of ECBBN at different pH values

261 was studied. The removal efficiency of RB19 (Fig. 9) at the lowest dose of sorbent
262 (250.0 mg dm⁻³) is low (36.36%). For higher sorbent doses of 500.0, 750.0
263 and 1000.0 mg dm⁻³, the removal efficiency of RB19 increases up to 74.73, 99.54
264 and 99.65%, respectively. A rapid increase in the efficiency of dye removal with
265 increasing sorbent dose occurs due to an increase in the surface area of the sorbent
266 and availability of more binding sites for RB19 [8, 49, 50]. Taking into considera-
267 tion sorption efficiency, sorption amount of dye and the cost of sorbent, a dose of
268 500.0 mg dm⁻³ of the sorbent is took as optimum and used for further experiments.

269 Effect of initial dye concentration on removal efficiency of RB19

270 Pollutant concentration is one of the most important parameters that can affect
271 the adsorption process. The effect of the initial dye concentration on the removal
272 efficiency was investigated by varying the concentration of RB19 from 100.0 to
273 700.0 mg dm⁻³ at constant sorbent dose (500.0 mg dm⁻³) and pH 2. The results are
274 presented in Fig. 10, and they show that the removal efficiency decreases from 99.65
275 to 74.73% with increasing initial concentration of dye from 100.0 to 700.0 mg dm⁻³.
276 The decrease in removal efficiency with increasing dye concentration occurs due to
277 the saturation of the limited available binding sites when using a constant sorbent
278 dose [51].

279 Kinetics study

280 Sorption kinetics study is very important for a complete understanding of the sorp-
281 tion behaviour. To evaluate the sorption mechanisms and identify the potential
282 rate-controlling steps, reaction and diffusion kinetic models were used to test the

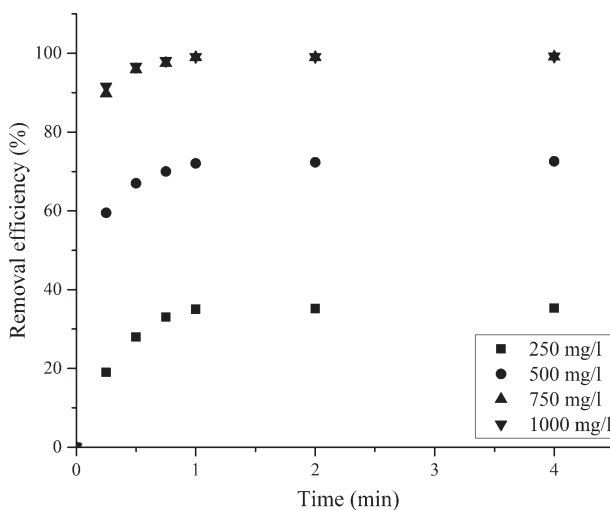


Fig.9 Effect of sorbent dose on the removal efficiency of RB19. c_{RB19} 700.0 mg dm⁻³, temperature 25.0 ± 0.5 °C, pH 2.0

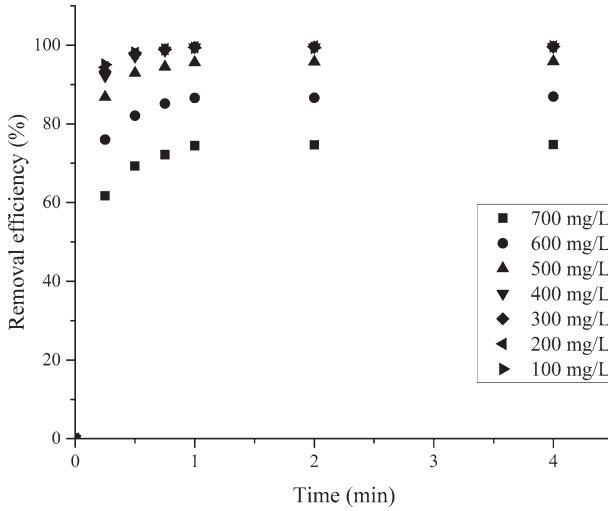


Fig. 10 Effect of initial concentration of dye on the removal efficiency of RB19; $c_{\text{sorbent}} 500.0 \text{ mg dm}^{-3}$, temperature $25.0 \pm 0.5 \text{ }^\circ\text{C}$, pH 2.0

283 experimental data. Pseudo-first-order and pseudo-second-order reaction kinetics
 284 models nonlinear form of equations are expressed as follows:

$$285 \quad q_t = q_e(1 - e^{-k_1 t}) \quad (4)$$

$$286 \quad q_t = \frac{q_e^2 k_2 t}{1 + k_2 q_e t} \quad (5)$$

287 where q_t is amount of dye sorbed at time t (mg g^{-1}), q_e (mg g^{-1}) is amount of dye
 288 sorbed at equilibrium state, k_1 (min^{-1}) and k_2 ($\text{g mg}^{-1} \text{ min}^{-1}$) are pseudo-first and
 289 pseudo-second-order reaction rate constants, respectively [52, 53].

290 The intraparticle diffusion model proposed by Weber and Morris was used for
 291 the description of the diffusion mechanism, and it is expressed by the following
 292 equation:

$$293 \quad q_t = k_{\text{id}} t^{1/2} + C \quad (6)$$

294 where k_{id} ($\text{mg g}^{-1} \text{ min}^{-1/2}$) is the intraparticle diffusion rate constant, q_t (mg g^{-1}) is
 295 the amount of RB19 sorbed at time t and C is the constant varied directly with the
 296 boundary layer thickness [54].

297 All the parameters, which characterize these models, were determined by nonlin-
 298 ear regression analysis of experimental data for pseudo-first-order and pseudo-sec-
 299 ond-order models and linear for the intraparticle diffusion model. Regression analy-
 300 sis was done using software OriginPro 2016, and results are presented in Table 3.

301 The determination coefficients for both reactions kinetic models are higher than
 302 0.999, which indicates that both models can be successfully applied for the sorption
 303 process. Similar values of the calculated q_e with experimentally determined $q_{e, \text{exp}}$

Table 3 Kinetic parameters for RB19 sorption onto ECBBN sorbent

c (mg dm ⁻³)	100	200	300	400	500	600	700
$q_{e, \text{exp}}$ (mg g ⁻¹)	199.32	398.63	597.27	796.58	959.02	1043.00	1046.24
Pseudo-first-order model							
q_e (mg g ⁻¹)	197.92	396.48	593.93	790.82	949.59	1027.01	1028.02
k_1 (min ⁻¹)	12.88	12.09	11.35	10.65	9.71	8.53	7.09
r^2	0.9999	0.9998	0.9998	0.9996	0.9995	0.9986	0.9981
RMD (%)	0.30	0.39	0.44	0.57	0.71	1.20	1.63
Pseudo-second-order model							
q_e (mg g ⁻¹)	200.96	403.95	607.22	811.93	981.47	1074.13	1093.96
k_2 (g mg ⁻¹ min ⁻¹)	0.36	0.15	0.08	0.05	0.03	0.02	0.01
r^2	0.9999	0.9999	0.9999	0.9998	0.9997	0.9996	0.9993
RMD (%)	0.27	0.28	0.37	0.44	0.53	0.65	0.76
Intraparticle diffusion model							
k_{i1} (mg g ⁻¹ min ^{-1/2})	296.40	591.45	882.33	1168.17	1391.82	1472.57	1437.58
C_1 (mg g ⁻¹)	9.50	18.53	26.88	34.66	39.01	39.79	32.90
r^2	0.9060	0.9115	0.9181	0.9140	0.9259	0.9229	0.9393
k_{i2} (mg g ⁻¹ min ^{-1/2})	1.06	1.80	2.70	4.61	9.12	13.50	22.62
C_2 (mg g ⁻¹)	197.20	395.43	592.50	788.26	942.45	1018.06	1005.96
r^2	0.9207	0.9297	0.9297	0.9388	0.9223	0.9301	0.9381

304 also confirms the applicability of these kinetic models. The obtained q_e values for
305 the pseudo-first-order model are in slightly better agreement with experimental data
306 in comparison with results obtained for the pseudo-first-order model. However, for
307 all tested concentrations lower RMD values for the pseudo-second-order than for the
308 pseudo-first-order model were obtained, which indicates that pseudo-second-order
309 model fitted the experimental data slightly better. Thus, obtained results suggest that
310 the rate-controlling step in the sorption process might be surface reaction through
311 electron sharing/exchange between RB19 and active sites of sorbent, ion exchange
312 reaction, complexation, coordination and/or chelation [55, 56]. A small specific
313 surface area of the sorbent also indicates that the above-mentioned processes have
314 a greater impact on the sorption process than the physical sorption. The values of
315 pseudo-second-order reaction rate constants, k_2 , decrease with increasing initial
316 RB19 concentration, because almost all available binding sites at the sorbent surface
317 are free at lower initial dye concentrations, resulting in high reaction rate constant
318 values. With higher dye concentrations, saturation of binding sites occurs, which
319 leads to a decrease of the k_2 values.

320 The results of linear regression analysis for the intraparticle diffusion model are
321 given in Table 3. The two linear ranges in the shape of the intraparticle diffusion
322 plot of q_t versus $t^{1/2}$ indicate that two steps occur in the adsorption process. The first,
323 sharp linear range can be ascribed to the external surface adsorption or instantaneous
324 adsorption stage of RB19 on the sorbent. When the adsorption onto the external
325 surface reaches saturation, the second linear range begins, which represents the
326 gradual adsorption stage, where the intraparticle diffusion is rate-controlled [57].

327 The first step is very fast, finished in about 1 min, while the second step is very slow,
 328 and after the first minute, the change of amount of sorbed dye is negligible. The
 329 intraparticle diffusion rate constant k_{i2} is much lower than k_{i1} , which confirms that
 330 the rate-limiting step is intraparticle diffusion through the boundary layer.

331 The results which show that both reaction models have very good agreement with
 332 experimental data and that the intraparticle model shows that the sorption process
 333 ends quickly (very small slope of the second linear part which starts after 1 min)
 334 prove enormous rate of sorption process with mixed control by surface reactions and
 335 diffusion.

336 Adsorption isotherms

337 The isotherm models were used for investigation of adsorption equilibrium
 338 between the ECBBN sorbent and textile dye RB19. Adsorption isotherms meas-
 339 urements were carried out by varying the RB19 concentration between 100.0 and
 340 700.0 mg dm⁻³ at pH 2.0. Several adsorption isotherms, such as Langmuir [58], Fre-
 341 undlich [59], Redlich–Peterson [60] and Brouers–Sotolongo [61, 62], were applied
 342 to simulate the experimental data. Langmuir model assumes monolayer adsorption
 343 at specific homogeneous surfaces on uniformly energetic adsorption sites, with no
 344 lateral interaction between adsorbed molecules. Freundlich model was applied to
 345 multilayer adsorption at a heterogeneous surface with non-uniform distribution of
 346 adsorption heat and affinities over the heterogeneous surface. The Redlich–Peterson
 347 isotherm is a combined form of Langmuir and Freundlich equations and assumes
 348 that adsorption does not follow ideal monolayer adsorption. Brouers–Sotolongo iso-
 349 therm model predicts adsorption at the heterogeneous surface. These adsorption iso-
 350 therms can be expressed in a nonlinear form by the following equations:

$$351 \quad q_e = \frac{q_m K_L c_e}{1 + K_L c_e} \quad (7)$$

$$352 \quad q_e = K_F c_e^{\frac{1}{n}} \quad (8)$$

$$353 \quad q_e = \frac{K_{RP} c_e}{1 + \alpha_{RP} c_e^\beta} \quad (9)$$

$$354 \quad q_e = q_m (1 - \exp(-K_W c_e^\alpha)) \quad (10)$$

355 where q_e (mg g⁻¹) is the amount of RB19 sorbed by the sorbent at equilibrium
 356 time; c_e (mg dm⁻³) is the concentration of RB19 at equilibrium time in solution; q_m
 357 (mg g⁻¹) is the maximum sorption capacity of sorbent; K_L (dm³ mg⁻¹) is Langmuir
 358 constant related to the energy of sorption, K_F ((mg g⁻¹) (dm³ mg⁻¹)^{1/n}) is Freundlich
 359 equilibrium constant, n is Freundlich exponent related to the intensity of sorption,
 360 K_{RP} (dm³ g⁻¹) is the Redlich–Peterson isotherm constant, α_{RP} is also a constant hav-
 361 ing unit of dm³ mg⁻¹, β is an exponent varied between 0 and 1, K_W (dm³ mg⁻¹) is

362 Brouers–Sotolongo isotherm constant and the dimensionless exponent α is a meas-
 363 ure of the width of the sorption energy distribution and therefore of the energy het-
 364 erogeneity of the surface.

365 These isotherms were characterized by parameters, which express affinity and
 366 surface properties of sorbents. All parameters of these isotherms models were deter-
 367 mined by nonlinear regression analysis using OriginPro 2016, and the results are
 368 given in Table 4.

369 Applicability of these models was determined by determination coefficients and
 370 relative mean deviations. The Langmuir, Redlich–Peterson and Brouers–Sotolongo
 371 sorption isotherms have very high r^2 values (higher than 0.98), while the Freun-
 372 dlich model has significantly lower determination coefficient (0.72) than these three
 373 models. In addition, RMD for the Freundlich model (16.57%) is the highest, which
 374 confirms that the sorption process does not follow the Freundlich isotherm. The
 375 other three models have much lower values of RMD , 3.14%, 3.19% and 3.85% for
 376 Langmuir, Redlich–Peterson and Brouers–Sotolongo, respectively. The obtained q_m
 377 for Langmuir model (1049.19 mg g⁻¹) is in slightly better agreement with experi-
 378 mental data (1046.24 mg g⁻¹) in comparison with q_m for Brouers–Sotolongo model
 379 (1014.86 mg g⁻¹). Based on r^2 , RMD and results for maximum sorption capac-
 380 ity, it can be concluded that among of all above-mentioned models Langmuir,
 381 Redlich–Peterson and Brouers–Sotolongo models can be used to describe sorption
 382 of RB19 on ECBBN sorbent, and for the nuance, Langmuir model has better match-
 383 ing with experimental results than the other models. The Redlich–Peterson exponent
 384 β is close to 1, and for that value these isotherm model is effectively reduced to the
 385 Langmuir model, which means that Langmuir will be preferable isotherm in compar-
 386 ison with Freundlich. Brouers–Sotolongo exponent α , which is in relation with
 387 the heterogeneity of the surface, is also close to 1 and indicates that adsorption sites
 388 of ECBBN sorbent are homogenous. Based on the applied isotherm models, it can
 389 be inferred that the sorption has homogenous character, which confirms good agree-
 390 ment with the Langmuir type of isotherm.

391 R_L is a dimensionless constant (commonly known as separation factor) derived
 392 from the Langmuir isotherm, which can be expressed as follows [63]:

Table 4 Isotherm parameters for RB19 sorption onto ECBBN sorbent

Adsorption isotherm	Parameter	Values	r^2	RMD (%)
Langmuir	K_L	0.91	0.9895	3.14
	q_m	1049.19		
Freundlich	K_F	515.14	0.7596	16.57
	n	6.37		
	Redlich–Peterson	K_{RP}		
	α_{RP}	0.86		
	β	1.01		
Brouers–Sotolongo	K_W	0.65	0.9851	3.85
	q_m	1014.86		
	α	0.93		

$$R_L = \frac{1}{1 + K_L c_0} \quad (11)$$

394 It describes the adsorption nature, which can be defined as unfavourable ($R_L > 1$),
 395 linear ($R_L = 1$), favourable ($0 < R_L < 1$) or irreversible ($R_L = 0$). The R_L values were
 396 found to be from 0.0108 to 0.0016 as the initial concentration of dye increases from
 397 100 to 700 mg dm⁻³. This means that the reaction is more favourable for high RB19
 398 concentrations. The value of Freundlich exponent ($1/n < 1$) confirms that adsorption
 399 is favourable.

400 **The mechanism of sorption of RB19 onto ECBBN sorbent**

401 According to all the results described in the manuscript, it can be concluded that
 402 the mechanism of RB19 sorption on ECBBN sorbent is complex, and the possible
 403 mechanism can be presented as follows. From the results of the influence of pH,
 404 it can be seen that the sorption capacity is the highest at pH 2 and it continually
 405 decreases with increasing pH to 9. However, at pH 9, the sorption capacity is still
 406 very high. Thus, it is obvious that electrostatic interactions, which mainly occur at
 407 low pH values, are not the only mechanism of the sorption process: the complexa-
 408 tion also affects the sorption process. Since sulphonic acids are very strong acids
 409 (their pK_a values are low), sulphonic groups of the RB19 dye will be dissociated
 410 ($-\text{SO}_3^-$) in the entire investigated range of pH. So, chemical interaction of sulphonic
 411 group of RB19 with polycation $[\text{Bi}_6\text{O}_5(\text{OH})_3]^{5+}$ of ECBBN occurs in the whole
 412 range of pH. In contrast, the contribution of physical sorption is small due to the
 413 small specific surface area of ECBBN, and therefore, mechanism of the sorption
 414 process is the most likely combination of electrostatic and chemical interactions
 415 between RB19 and ECBBN sorbent.

416 **Treatment of a model solution of polluted Nišava River water**

417 In order to investigate the applicability of ECBBN in the purification of real pol-
 418 luted water, treatment of a model solution of river water contaminated with RB19
 419 was done. The river water samples were collected from Nišava River and were used
 420 without further treatment, except the filtration through 0.45 μm regenerated cellu-
 421 lose membrane filter. The river water was used as the matrix of the solutions used
 422 in the experiments. A model solution of polluted river water was made by adding
 423 500.0 mg dm³ of RB19 to the matrix. According to the previous results, experiments
 424 were done at optimal conditions by using a sorbent dose of 500.0 mg dm³ and at pH
 425 2.0. Results (Fig. 11) show that the removal efficiency of RB19 from model solution
 426 of contaminated river water is also high, but the sorption capacity, as expected, is
 427 slightly lower than in model solution made with deionized water. Sorption capacity
 428 in the model solution of polluted river water was 838.25 mg dm³, which is 19.88%
 429 lower in comparison with the deionized water model solution. This may be attrib-
 430 uted to the presence of organic matter in the river water, which can be also sorbed
 431 at the active sites of ECBBN sorbent. The high sorption capacity of ECBBN for the

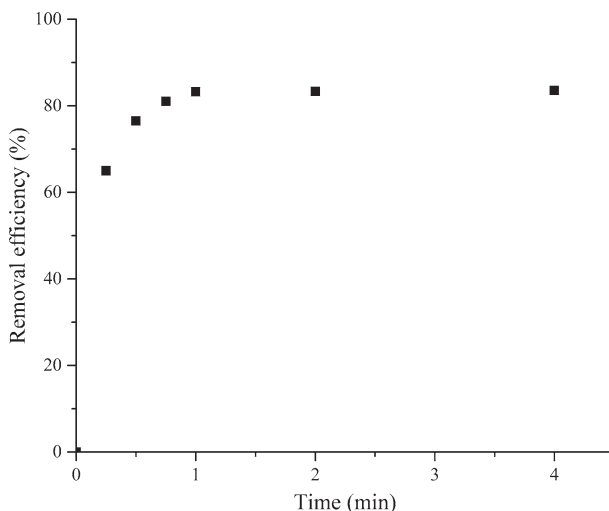


Fig. 11 Effect of contact time on the removal efficiency of RB19 in the model solution of polluted river water. c_{RB19} 500.0 mg dm⁻³, $c_{sorbent}$ 500.0 mg dm⁻³, temperature 25.0 ± 0.5 °C, pH 2.0

432 removal of RB19 from the river water indicates that this material can be suitable
 433 sorbent for the textile dyes removal from real polluted water.

434 **Conclusions**

435 Pure basic bismuth nitrate [Bi₆O₅(OH)₃](NO₃)₅·2H₂O was, for the first time, suc-
 436 cessfully synthesized by electrochemical deposition, followed by thermal treatment
 437 at 200 °C. The chemical structure of ECBBN was ascertained by XRD, FTIR and
 438 EDX analyses. The material is composed of small crystals forming high aggre-
 439 gates; the crystallite size is 11.3 ± 0.2 nm. Sorption of RB19 by electrochemically
 440 synthesized sorbent (ECBBN) is very fast (above 95% of the total sorption at equi-
 441 librium was reached in 1 min). Sorption kinetics shows that both surface reaction
 442 and diffusion were rate-limiting steps. Based on the determination coefficients and
 443 relative mean deviations it can be deduced that the experimental data were the best
 444 fitted with Langmuir isotherm. The maximum sorption capacity (1049.19 mg g⁻¹)
 445 was achieved at pH 2.0. Very high sorption capacity and fast equilibration are very
 446 important characteristics for the potential practical use of ECBBN, as well as high
 447 sorption capacity in model solutions of contaminated river water. The removal effi-
 448 ciency of RB19 increases with increasing sorbent dose and decreasing dye concen-
 449 tration. Low cost, eco-friendly starting materials, simple and non-time consuming
 450 synthesis method, high purity and repeatability of the synthesized material structure,
 451 as well as very high sorption capacity, better sorption performance and lower sorp-
 452 tion equilibrium time than similar materials, make ECBBN sorbent a very attractive
 453 system for the removal of textile dyes from polluted water.

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