

Field-effect control of Graphene-Fullerene thermoelectric nanodevices

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Abstract

Although it was demonstrated that discrete molecular levels determine the sign and magnitude of the thermoelectric effect in single-molecule junctions, full electrostatic control of these levels has not been achieved to date. Here, we show that graphene nanogaps combined with gold micro-heaters serve as a testbed for studying single-molecule thermoelectricity. Reduced screening of the gate electric field compared to conventional metal electrodes allows controlling the position of the dominant transport orbital by hundreds of meV. We find that the power factor of graphene-fullerene junctions can be tuned over several orders of magnitude to a value close to the theoretical limit of an isolated Breit-Wigner resonance. Furthermore our data suggests that the power factor of isolated level is only given by the tunnel coupling to the leads and temperature. These results open up new

15 **avenues for exploring thermoelectricity and charge transport in individual molecules, and**
16 **highlight the importance of level-alignment and coupling to the electrodes for optimum**
17 **energy-conversion in organic thermoelectric materials.**

18 **Introduction**

19 The thermopower or Seebeck coefficient S of a material or nanoscale device is defined as $S =$
20 $-\Delta V/\Delta T$, where ΔV is the voltage difference generated between the two ends of the junction
21 when a temperature difference ΔT is established between them. In addition to the goal of
22 maximising S , there is a great demand for materials with a high power factor S^2G , which
23 is a measure for the amount of energy that can be generated from a temperature difference,
24 and high thermoelectric efficiency, which is expressed in terms of a dimensionless figure of
25 merit $ZT = S^2GT/\kappa$, where T is the average temperature, G is the electrical conductance
26 and κ is the sum of the electronic and phononic contribution to the thermal conductance. In
27 conventional thermoelectric materials S , G and κ are typically mutually contra-indicated, such
28 that high S is accompanied by low G and high G by high κ ¹. In some nanostructured materials
29 these properties can be decoupled². Therefore, the thermoelectric properties of nanostructures
30 like carbon nanotubes³, quantum dot devices⁴⁻⁶, and single-molecule junctions⁷⁻¹⁴ have been
31 studied extensively. In the past few years it has been demonstrated both experimentally and
32 theoretically that, at the molecular scale, S can be controlled by the chemical composition¹⁰, the
33 position of intra-molecular energy levels relative to the work function of metallic electrodes¹²,
34 by systematically increasing the single-molecule lengths within a family of molecules^{9,11}, and
35 by tuning the interaction between two neighbouring molecules⁸. Despite these advances, single-
36 molecule experiments have only yielded values of S ranging from 1 to 50 $\mu\text{V K}^{-1}$ ^{7,15}. The key
37 challenge in achieving high Seebeck coefficients in molecular junctions lies in controlling the
38 energetic position and “steepness” of the transport resonances.

39 We use graphene-based lateral single-molecule devices – where a molecule sits in the gap
40 between two graphene leads – to study the gate-dependent thermoelectric properties of C₆₀
41 molecules. The two-dimensional nature of graphene electrodes leads to a reduced screening
42 of the gate electric field compared to bulky metal electrodes¹⁶, enabling us to shift the orbital
43 energy levels of the molecule with respect to the electrochemical potential of the graphene leads
44 using a back-gate. We exploit this field-effect control to map the thermo-voltage across entire
45 molecular transport resonances.

46 **Experimental part**

47 Our devices consist of CVD graphene etched into bow-tie shape on-top of gold contacts (see
48 Methods for fabrication details). Each gold lead has four contacts for precise 4-terminal resis-
49 tance measurements, which allows us to measure the temperature difference across the graphene
50 junction (see Figure S1). A gold micro-heater is fabricated 1 μm away from the junction (see
51 Figure 1a). By passing a current through the micro-heater we create a temperature gradient
52 across the junction^{3,17,18}. We quantify this temperature gradient by cross-checking several met-
53 hods to eliminate potential systematic errors. These are: (i) measuring the resistance of the left
54 and right gold contacts; (ii) using COMSOL finite-element simulations; and (iii) using Scan-
55 ning Thermal Microscopy (SThM) measurements. Using method (i) we measure a temperature
56 difference between the hot (closer to the micro-heater) and cold (further from the micro-heater)
57 contact as a function of heater power $\Delta T/P_{\text{heater}} = 58 \pm 11 \text{ K W}^{-1}$ at $T_0 = 77 \text{ K}$ (see Chap-
58 ter 1 and 8 Supporting Information for details of the calibration method and an estimation of
59 the total uncertainty, respectively). This is in close agreement with the finite-element simu-
60 lations (method (ii)) which predict $\Delta T/P_{\text{heater}} = 50 \text{ K W}^{-1}$ and a constant temperature gra-
61 dient $\nabla T/P_{\text{heater}} = 14 \text{ K } \mu\text{m}^{-1} \text{ W}^{-1}$ across the length of the graphene junction (see Figure
62 S5). Figure 1b shows a temperature map overlaid onto a height profile that were simultane-

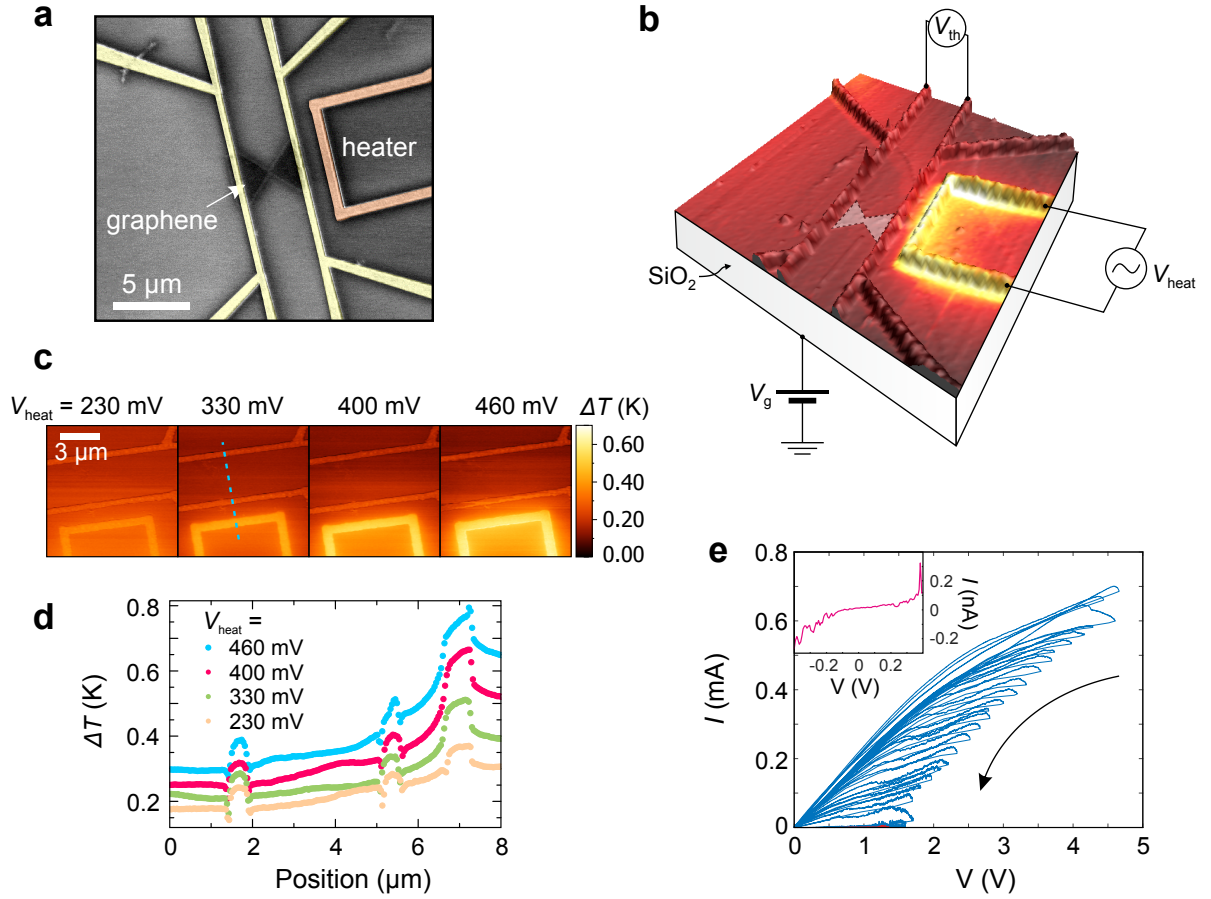


Figure 1: Device geometry and Scanning Thermal Microscopy. **a**, False-colour scanning electron microscopy image of the device. **b**, Atomic force microscopy height profile overlaid with scanning thermal microscopy signal and sketch of the device geometry for a typical thermo-voltage measurement. **c**, Scanning thermal microscopy images recorded at different constant voltages V_{heat} applied to the micro-heater. **d**, Line profiles along the device extracted from the maps shown in **c** (see blue dotted line). **e**, IV_{sd} traces recorded during feedback-controlled electroburning. Inset: IV_{sd} trace after completed electroburning.

63 ously recorded using a SThM (method (iii)). From the temperature maps recorded for dif-
 64 ferent heater powers in Figure 1c and d we extract a power-dependent temperature gradient
 65 $\nabla T/P_{\text{heater}} = 18 \text{ K } \mu\text{m}^{-1} \text{ W}^{-1}$ and a temperature difference $\Delta T/P_{\text{heater}} = 63 \pm 10 \text{ K W}^{-1}$
 66 between the two gold contacts under ambient conditions and $\Delta T/P_{\text{heater}} = 71 \pm 11 \text{ K W}^{-1}$ for
 67 77 K and vacuum (see Chapter 3 Supporting Information). For all the analysis presented below

68 we will use the value extracted using method (i).

69 We use feedback-controlled electroburning^{19–22} (see Figure 1e) to first form graphene nano-
70 gaps suitable for characterisation of single molecules²³ in which we subsequently couple C₆₀
71 molecules functionalised with pyrene anchor groups (see Figure 2a). We have chosen this mole-
72 cule since it is stable in air, has previously been successfully coupled to graphene electrodes²⁴,
73 and because its thermoelectric properties have been studied using various other techniques,
74 including STM based break junctions^{8,12} and electromigrated gold break junctions⁷. After elec-
75 troburning we characterise the graphene gaps by measuring the current I_{sd} as a function of gate
76 and bias voltage (stability diagram) at $T_0 = 77$ K in vacuum. Empty devices, where there are
77 no carbon islands or ribbons bridging the gap, are characterised by non-linear $I_{sd} - V_{sd}$ curves
78 and little or no gate modulation. After this first characterisation step we warm up the device
79 and deposit C₆₀ molecules by immersing the sample in a 10 μ M chloroform solution containing
80 the C₆₀ bisadducts for 1 min followed by blow drying with nitrogen gas. We then measured
81 the devices again at low temperature to look for signatures of molecules. In total we fabricated
82 1080 two-terminal devices on which we performed feedback controlled electroburning. Due
83 to limitations of our setup we were then only able to study 100 devices at low temperatures of
84 which 16 devices showed signatures of molecule deposition: 1) a clear change from “empty”
85 to Coulomb blockade after molecule deposition; 2) vibrational fingerprints in the excited state
86 spectrum measured in the sequential tunneling regime.

87 **Results and discussion**

88 We often observe multiple overlapping, non-closing Coulomb diamonds which indicate the for-
89 mation of molecular junctions where more than one molecule contribute to the electrical trans-
90 port. In the following we discuss the data for 3 selected devices where the Coulomb diamonds
91 close in the accessible back-gate region with addition energies > 400 meV. We focus on these

92 devices as their transport is most likely dominated by a single molecule. Moreover, the large
 93 addition energies enables us to study well isolated energy levels that are expected to show the
 94 largest Seebeck coefficient. Chapter 5 of the Supporting Information includes the data of all
 measured devices.

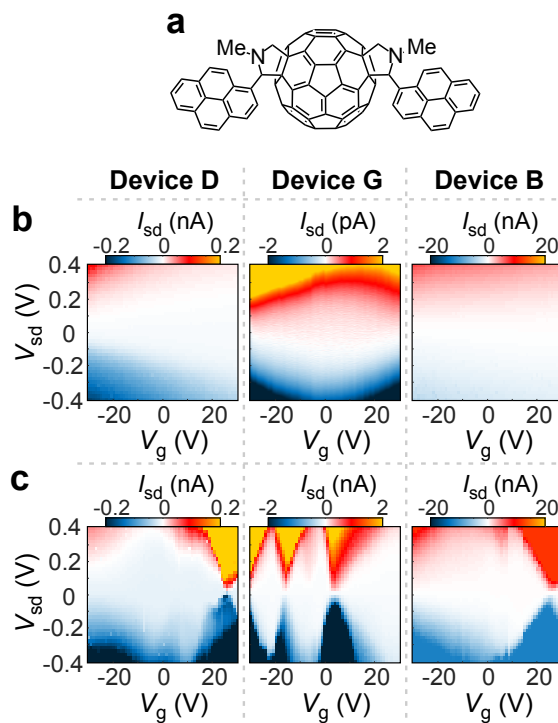


Figure 2: Electrical characterisation of Graphene-Fullerene Single-Molecule thermoelectric nanodevices. (a) Chemical structure of the C₆₀ bisadducts functionalised with pyrene anchor groups. (b) Current map as a function of back gate and bias voltage before and (c) after molecule deposition recorded at $T_0 = 77$ K for devices D, G and B, respectively.

95

96 Figure 2b shows the stability diagrams of devices B, D and G measured at 77 K before
 97 and after molecule deposition. In Figure 2b, before molecule deposition, the source-drain cur-
 98 rent shows only weak gate dependence, but in Figure 2c regions of Coulomb blockade can be
 99 observed after deposition. We attribute the sequential electron tunneling after molecule depo-
 100 sition to the formation of a molecular junction.^{19,23,24} To further investigate the single electron
 101 transport, we studied several devices at low temperatures ($T < 5$ K). In a previous study we ob-

102 served excited state lines in the sequential tunneling regime that correspond to $H_g(1)$ and $A_g(1)$
103 Raman active vibrational modes of C_{60} as well as centre-of-mass motion of the C_{60} molecule
104 with respect to the graphene electrodes.²⁴ In total, 7 of 16 devices showed similar evidence for
105 vibrational excited states (see Table S2 Supporting Information). 4 out of 16 devices changed
106 permanently to a non-conducting state after cool down to < 5 K and no low-temperature data
107 could be recorded. The visibility of vibrational excited states strongly depends on temperature,
108 the tunnel coupling to the leads²⁵ and the Franck-Condon factors^{26,27} which can vary drasti-
109 cally between different molecular junctions and the charge-transition investigated.^{24,28} Moreo-
110 ver, density of states fluctuations in the graphene leads can lead to features inside the sequential
111 tunneling regime, which do not run parallel to the edges of the Coulomb diamonds, that can
112 obscure any vibrational fingerprint.²⁹

113 Next, we measure the gate dependent thermoelectric properties of the C_{60} -graphene juncti-
114 ons. We apply an AC-voltage with modulation frequency f to the micro-heater and measure
115 the thermo-voltage V_{th} drop on the device at a frequency $2f$ for different back gate voltages V_g
116 (see Figure 1b).¹⁷ We focus on the high-conductance gate region around the Coulomb peaks
117 (see gate traces in Figure 3a) since the thermo-voltage signal inside the Coulomb blocked re-
118 gion is smaller than the noise level of our measurement setup. Figure 3b shows the measured
119 gate-dependend thermo-voltage signal for Device D, G and B, recorded at $\Delta T = 45 \pm 9$ mK,
120 $\Delta T = 100 \pm 20$ mK and $\Delta T = 180 \pm 36$ mK, respectively. An increase of V_{th} followed by a
121 sign change, further decrease and subsequent increase towards zero can be observed. Similar
122 results have been observed for 7 other devices (see Chapter 5 Supporting Information). Using
123 the applied temperature bias ΔT we find maximum Seebeck coefficients S_{max} ranging from 1.5
124 to $460 \mu\text{V K}^{-1}$ (see Table 1). On average, these values are more than one order of magnitude
125 larger than the Seebeck coefficients found in STM break junction experiments of C_{60} contacted
126 with different metal electrodes^{8,12}. In the following we use a simple model for an isolated

127 Breit-Wigner resonance to explain these results.

128 In the linear temperature and bias regime the conductance G can be expressed in terms of
 129 the moments L_i of the transmission coefficient $P(E)$ as³⁰

$$G(V_g, T_0) = \frac{2e^2}{h} L_0 \quad (1)$$

130 with

$$L_i = \int_{-\infty}^{\infty} (E - E_F)^i P(E) dE, \quad (2)$$

131 where we use the non-normalised probability distribution³¹

$$P(E) = -\mathcal{T}(E) \frac{\partial f(E)}{\partial E}. \quad (3)$$

132 For a single, well isolated molecular level we can assume a Breit-Wigner resonance to describe
 133 the transmission probability $\mathcal{T}(E)$:

$$\mathcal{T}(E) = \frac{\Gamma_L \Gamma_R}{(\Gamma_L/2 + \Gamma_R/2)^2 + [(e\alpha V_g - E_0) - E]^2}, \quad (4)$$

134 where E_0 is the energy of the transport resonance, Γ_L, Γ_R are the tunnel couplings to the leads,
 135 and the lever arm $\alpha = \frac{dE}{dV_g}$ is determined by the capacitive coupling of the molecule to the gate,
 136 source and drain electrodes³². The derivative of the Fermi-Dirac distribution is

$$\frac{\partial f(E)}{\partial E} = \frac{1}{4kT_0} \cosh^{-2} \left(\frac{E}{2kT_0} \right). \quad (5)$$

137 In the limit where $\Gamma = \Gamma_L + \Gamma_R \gg k_B T_0$ Equation (1) reduces to $G = \frac{2e^2}{h} \mathcal{T}(E)$, and the
 138 tunnel coupling to the two leads can be inferred from the height and width of the Coulomb peak.
 139 In the opposite limit where $\Gamma \ll k_B T_0$ the maximum conductance G_{\max} is proportional to $\frac{\Gamma_L \Gamma_R}{\Gamma_L + \Gamma_R}$
 140 while the width of the Coulomb peak is proportional to $k_B T_0$.

141 When a temperature bias ΔT is applied to a junction, the Fermi-Dirac distribution of the hot
 142 contact broadens compared to that of the cold contact. This gives rise to a thermal current I_{th} ,

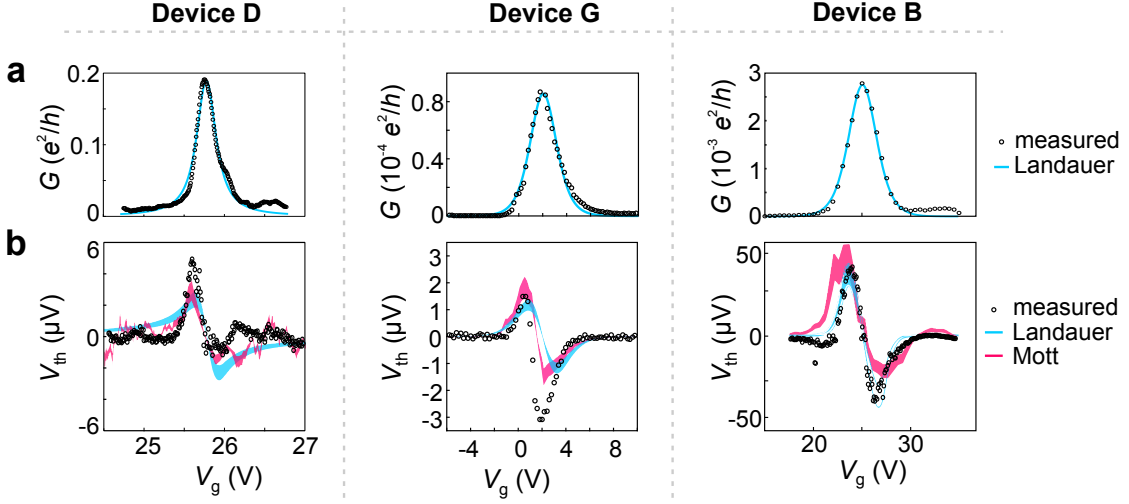


Figure 3: **Thermoelectric measurements.** (a) AC Zero-bias conductance and (b), Thermo-voltage (measured with a temperature bias of $\Delta T = 45 \pm 9$ mK, $\Delta T = 100 \pm 20$ mK and $\Delta T = 180 \pm 36$ mK, respectively) as a function of back gate voltage measured at $T_0 = 3.2$ K (Device D) and $T_0 = 77$ K (Device G and B). The blue and pink curves show theoretical calculations using a Landauer-type approach and the Mott formula, respectively.

Table 1: Measurement results for each C_{60} device.

| Device name | Γ (μeV) | χ | α (meV/V) | E_0 (meV) | S_{max} ($\mu\text{V/K}$) | G_{max} (e^2/h) | $(S^2G)_{\text{max}}$ (k_{B}^2/h) | T_0 (K) |
|-------------|-----------------------------|-------------------|-----------------------------|------------------------|--------------------------------------|------------------------------|--|-----------|
| B | 88 | – | 9 | 221 | 220 | 0.003 | 0.01 | 77 |
| C | 1.3×10^3 | – | 10 | 188 | 140 | 0.08 | 0.08 | 77 |
| D | 2.7×10^3 | 15 | 13 | 335 | 27 | 0.2 | 0.14 | 3.2 |
| E | 16 | – | 6 | 53 | 238 | 0.006 | 0.02 | 11 |
| F | 1.7×10^2 | – | 11 | 84 | 460 | 0.01 | 0.11 | 77 |
| G | 2 | – | 9 | 12 | 30 | 10^{-4} | 0.04 | 77 |
| Q | 2.4×10^4 | 1.2×10^4 | 62 | 564 | 1.5 | 2×10^{-4} | 7×10^{-4} | 77 |

143 which leads to a thermo-voltage V_{th} when measured under open circuit conditions $I(\Delta T, V_{\text{th}}) =$
144 0. The ratio of the thermo-voltage and the temperature drop is the Seebeck coefficient $S =$
145 $-V_{\text{th}}/\Delta T$. Similar to the conductance, the Seebeck coefficient is given by a Landauer-type
146 expression using Equation 2, 3 and 5:

$$S(V_g, T_0) = -\frac{1}{eT_0} \frac{L_1}{L_0}. \quad (6)$$

147 If $\mathcal{T}(E)$ varies only slowly with E on the scale of $k_B T_0$, i.e. $\Gamma \gg k_B T_0$, then S takes the
 148 well-known form of the Mott approximation³³

$$149 \quad S = -\frac{\pi^2 k_B^2 T_0}{3e\alpha} \frac{1}{G} \frac{dG}{dV_g}, \quad (7)$$

150 In Figure 3b we compare our experimental results to the calculated thermo-voltages using
 151 the Mott approximation (equation 7) and the Landauer-type approach (equation 6), respecti-
 152 vely, where the width of the curve indicates the error in estimating the temperature drop on the
 153 junction (see full error analysis in Chapter 8 Supporting Information). For both calculations the
 154 thermo-voltage was corrected by a damping factor due to the input impedance of the voltage
 155 amplifier (see Chapter 8.4 Supporting Information)⁵. To compare the measured thermo-voltage
 156 to that obtained from Equation 6 and 7 we assume that the temperature difference ΔT bet-
 157 ween the hot and the cold side of the molecule is equal to the temperature difference measured
 158 between the two gold contacts. Since cooling lengths of up to $7\mu\text{m}$ have been reported for
 159 graphene³⁴, the assumption that hot electrons injected from the gold contacts into the graphene
 160 leads do not thermalise before they reach the junction area approximately $1.7\mu\text{m}$ away from the
 161 gold contacts is justified. By assuming that no temperature drops on the graphene leads we only
 162 estimate a lower bound of S . In addition, we neglect the effect of thermo-voltages created in
 163 the strongly p-doped graphene leads whose Seebeck coefficient is on the order of $10\mu\text{V}/\text{K}$ ¹⁷.
 164 However, this would result in a small, constant offset of the thermo-voltage in the applied gate
 165 voltage regime far away from the Dirac point of our graphene,²² which we do not observe in
 166 our experiments.

167 For the calculation of the Seebeck coefficient using the Landauer-type approach (equation 6)
 168 we estimate $\mathcal{T}(E)$ by equation 4 and extract the tunnel coupling by fitting the gate-dependent
 169 conductance traces to Equation 1 if $\Gamma \gg k_B T_0$. For those devices where $\Gamma \ll k_B T_0$, we
 170 estimate $\mathcal{T}(E)$ by fitting the conductance data with a thermally broadened conductance peak

171 $G = G_{\max} \cosh^{-2} [(\alpha V_g - E_0)/(2k_B T_0)]$ with $G_{\max} = e^2/(\hbar 4k_B T) \Gamma_L \Gamma_R / (\Gamma_L + \Gamma_R)$,³⁵ where
 172 we fix $T_0 = 77$ K, and find a lower bound for Γ by taking $\Gamma_L = \Gamma_R$ such that $\Gamma_{\text{lower}} =$
 173 $4k_B T_0 \frac{2\hbar}{\pi e^2} G_{\max}$. Despite the fact that we can not uniquely determine Γ in this regime, there
 174 is still good agreement between the measured and calculated thermo-voltage curves. This is
 175 due to the relative insensitivity of S on the lifetime of the transport resonance when $\Gamma \ll k_B T_0$
 176 (see Figure S22).

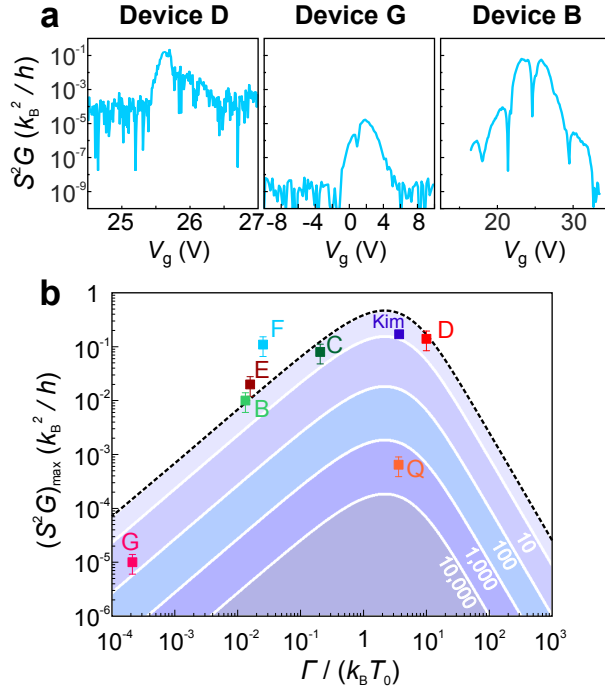


Figure 4: **Maximum power factor.** (a) Power factor as a function of back gate voltage measured at $T_0 = 3.2$ K (Device D) and $T_0 = 77$ K (Device G and B). (b) Maximum power factor as a function of tunnel coupling Γ for the devices investigated in this study and by Kim *et al.*⁷. The dashed black line ($\chi = 1$) and the white lines show theoretical curves calculated using Equation 8 for different ratios between the fast and slow tunnel rates χ . The error bars of the data points are estimated by neglecting the error in G and using the relative error in determining ΔT (20 %) to estimate the error for S . The total error of the power factor $PF = S^2G$ is propagated: $\Delta PF = \sqrt{\left(\frac{\partial PF}{\partial S} \Delta S\right)^2} = 2SG\Delta S = 2S^2G \frac{\Delta S}{S}$.

177 Finally, we use our experimental results to calculate the power factor S^2G for Devices D,

178 G and B (see Figure 4a and Chapter 5 Supporting Information for other devices). Significantly,
 179 we find that S^2G can be tuned by several orders of magnitude by electrical gating to maximum
 180 values of $0.01 - 0.14 \times k_B^2/h$ (see Table 1). These values are one to two orders of magnitude
 181 larger than values found in C_{60} junctions without sufficient electric field control^{8,12,14} and com-
 182 parable to the value found for C_{60} measured using gold break junctions with an electrical back
 183 gate⁷.

184 To evaluate the thermoelectric performance of different devices, we plot the maximum po-
 185 wer factor $(S^2G)_{\max}$ on a log-log scale as a function of the temperature-normalized tunnel rate
 186 $\Gamma/k_B T_0$. We compare these values to the theoretical maximum calculated using

$$187 \quad S^2G = \frac{2}{hT_0^2} \frac{L_1^2}{L_0}, \quad (8)$$

188 and Equations 1 - 6. In addition to the theoretical maximum power factor for devices with
 189 symmetric tunnel coupling (black dashed line), we plot the theoretical values for $(S^2G)_{\max}$ for
 190 different ratios between the fast and slow tunnel rates $\chi = \Gamma_{\text{fast}}/\Gamma_{\text{slow}}$ (solid white lines), where
 191 $\Gamma_{\text{fast}} = \max(\Gamma_L, \Gamma_R)$ and $\Gamma_{\text{slow}} = \min(\Gamma_L, \Gamma_R)$. For devices in the regime where $\Gamma \ll k_B T_0$
 192 we use the lower bound Γ_{lower} as described above. Since the maximum power factor in this
 193 regime is independent of the asymmetry between the fast and slow tunnel coupling (see Figure
 194 S21), the measured power factor for these devices are expected to fall on the black dashed line
 195 corresponding to $\chi = 1$. For the device where $\Gamma \ll k_B T_0$ G, B, E, F and C, we observe an
 196 increase of $(S^2G)_{\max}$ with increasing Γ_{lower} due to the power factor being proportional to G_{\max} .
 197 As Γ approaches $k_B T_0$ the power factor reaches a maximum $S^2G \approx \frac{1}{2.2} \times k_B^2/h$ for $\Gamma \approx 2.2k_B T_0$.
 198 Devices D and Q were measured close to this maximum, as was the C_{60} molecule measured by
 199 Kim *et al.* at 100 K denoted ‘Kim’ in Figure 4b.⁷ While devices D and ‘Kim’ have a power
 200 factor close to the theoretical limit, for device Q $(S^2G)_{\max}$ is several orders of magnitude lower
 201 as a result of the asymmetric coupling $\chi \approx 10^4$ in this device. For $\Gamma \gg k_B T_0$ the maximum

202 power factor is expected to decrease with increasing Γ as the lifetime broadening reduces the
203 Seebeck coefficient. No devices were measured in this regime.

204 Based on our finding, we conclude that there are three desiderata for achieving high ther-
205 moelectric performance in molecular nanodevices. First, the molecular energy levels need to
206 align closely with the Fermi level of the electrodes since the Seebeck coefficient is maximum
207 for E close to the centre of the transmission resonance. Second, the tunnel coupling needs to be
208 such that the lifetime of the transmission resonance is comparable to $k_B T_0$ at the operating tem-
209 perature. Third, the tunnel couplings to the left and right electrode need to be equal to achieve
210 a maximum power factor.

211 To summarise, we have fabricated thermoelectric nanodevices in which fullerene molecules
212 are anchored between graphene source and drain leads. We demonstrate that by applying a
213 thermal bias across the junction we can measure a gate dependent thermoelectricity. Our results
214 show that by carefully tuning the transmission of a molecular junction towards sharp isolated
215 resonance features, high power factors can be achieved approaching the theoretical limit of a
216 thermally and lifetime broadened Coulomb peak. These results are relevant for the development
217 of organic thermoelectric materials and our approach could also be applied to test hypotheses
218 about the thermoelectric properties of molecules exhibiting quantum interference effects³⁰ and
219 spin caloritronics³⁶.

220 **Methods**

221 **Device fabrication**

222 Our devices are fabricated from single-layer CVD-grown graphene, which we transfer onto a
223 Si/300 nm SiO₂ wafer with prepatterned 10 nm Cr/70 nm Au contacts and microheater. We
224 pattern the graphene into a bow-tie shape (see Figure 1a) using standard electron beam litho-
225 graphy and O₂ plasma etching. The channel length L of the devices and the width W of the

226 narrowest part of the constriction are $3.5 \mu\text{m}$ and 200 nm , respectively. To narrow down the
227 constriction or form a nanogap we use a feedback-controlled electroburning technique in air²²
228 using an ADWin Gold II card with a 30 kHz sampling rate. Electroburning cycles are repeated
229 until a critical resistance of $500 \text{ M}\Omega$ is reached.

230 **Scanning thermal microscopy temperature measurements**

231 This method uses a temperature sensitive calibrated microfabricated probe with an apex of a few
232 tens of nm that is brought in direct solid-solid contact with the sample. The SThM response V_t is
233 a linear function of the local sample temperature T_s . For a flat sample surface and constant tip-
234 surface thermal resistance (that is the case when the tip is in contact with the same material e.g.
235 SiO_2) it allows to directly map a 2D distribution of the temperature increase in the vicinity of the
236 micro-heater ΔT_s , as well as to obtain an absolute value of the sample temperature increase due
237 to micro-heater actuation using the following two quantitative methods: 1) In the null-method
238 the probe apex temperature T_a is varied, as the probe is brought repeatedly into contact with the
239 sample. The value at which no change in the probe response V_t occurs corresponds to $T_s = T_a$,
240 which provides an absolute temperature measurement with an error of about 15 % (see Chap-
241 ter 2 and 3 Supporting Information for details). 2) In the SThM addition method the sample
242 is heated both by the micro-heater as well as by the calibrated raise in the temperature of the
243 sample stage, allowing to perform measurements under vacuum and variable sample tempera-
244 tures (see Chapter 2 and 3 Supporting Information for more details). These measurements show
245 good correlation of the experimentally measured temperature maps with the finite-elements mo-
246 dels. SThM measurements under ambient conditions were performed using a commercial SPM
247 (BrukerMultiMode with Nanoscope E controller) and a custom-built SThM modified AC Whe-
248 atstone bridge. A resistive SThM probe (Kelvin Nanotechnology, KNT-SThM-01a, 0.3 N/m
249 springconstant, $< 100 \text{ nm}$ tip radius) served as one of the bridge resistors allowing precise mo-

250 nitoring of the probe AC electrical resistance at 91 kHz frequency via lock-in detection of the
251 signal (SRS Instruments, SR830) as explained elsewhere³⁷. Surface temperature maps were
252 obtained at varying DC current to the probe that generated variable Joule heating of the probe
253 tip. Several driving currents were used ranging from 0.10 to 0.40 mA leading to excess probe
254 temperatures up to 34 K. The probe temperature - electrical resistance relation was determined
255 employing a calibrated Peltier hot/cold plate (Torrey Pines Scientific, Echo Therm IC20) using
256 a ratiometric approach (Agilent 34401A)³⁷. The double-scan technique was used with different
257 probe driving currents in order to obtain quantitative measurements of the surrounding and of
258 the heater temperature³⁸. Laser illumination on the probe (on the order of 5 K) added to the
259 Joule heating and was accounted via measurement of corresponding probe resistance change.
260 SThM thermal mapping was performed with a set-force below 15 nN during imaging to protect
261 the tip and the sample from damage.

262 **Electric and thermoelectric transport measurements**

263 Graphene nano-structures were characterised in an Oxford Instruments Triton 200 dilution ref-
264 rigerator with 20 mK base temperature. All measurements on C₆₀ junctions were performed
265 in a liquid nitrogen dip-stick setup. Electrical DC transport measurements were performed
266 using low-noise DC electronics (Delft box). To measure the thermoelectric properties of nano-
267 structures we used the $2f$ method³. To this end an AC heater voltage $V_{\text{heat}}(f)$ with frequency f
268 was applied to the micro-heater using a HP33120a arbitrary waveform generator. The thermo-
269 voltage was measured with a SR560 voltage pre-amplifier and a SRS830 lock-in amplifier at a
270 frequency $2f$ (see Chapter 7 Supporting Information for more details).

271 **Supporting Information Available**

272 Calibration of the heater: Resistance method; Calibration of the heater: Scanning thermal mi-
273 croscopy; Calibration of the heater: Vacuum and variable temperature Scanning thermal mi-
274 croscopy; Calibration of the heater: COMSOL simulations; Supporting thermoelectric data:
275 C_{60} junctions; Maximum power factor; Details on thermovoltage measurements; Error analy-
276 sis.

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286 **Competing financial interests**

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288 **References and Notes**

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